Parameterizing The California Workers Compensation Experience Rating Plan: Development of Primary and Excess Credibilities & Translation into B and W Rating Values

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## PARAMETERIZING THE CALIFORNIA WORKERS COMPENSATION EXPERIENCE RATING PLAN

## DEVELOPMENT OF PRIMARY AND EXCESS CREDIBILITIES & TRANSLATION INTO B AND W RATING VALUES

## WARD BROOKS

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#### Abstract

This paper documents the methodology used to develop the primary and excess credibilities which underlie the experience rating plan of the Workers' Compensation Insurance Rating Bureau of California (the Bureau) and the translation of these credibilities into the B and W rating values used in the experience rating formula. The method is demonstrated with an analysis based on projecting experience modifications for policy year 1991. This analysis was completed in 1998 as part of the Bureau's regular maintenance of the Experience Rating Plan. The basic approach is one of multivariate regression but with the use of ridge regression to address the multicollinearity between the primary and excess components. Empirical results are smoothed by fitting logistic cumulative density functions. A process of iterative parameter refinement based on an extension of the traditional quintiles test is used and the performance of each iteration is assessed based on a neasure of plan efficiency.

## 1. INTRODUCTION

## Preliminaries

We will begin with a brief review of the experience rating formula currently used in California. The formula is:

(1)	Modification	= <u>Ap+</u>	$\frac{B+W\cdot Ae+(1-W)\cdot Ee}{E+B}  \text{or}  \frac{Ap+B+W\cdot Ae+(1-W)\cdot Ee}{Ep+B+W\cdot Ee+(1-W)\cdot Ee}$
	where Ap Ae	=	actual primary losses the excess of a risk's actual losses over the actual primary losses
	Ep	=	expected primary losses based on the appropriate D Ratios
	E	=	the excess of a risk's expected losses over expected primary losses expected total losses (Ep + Ee)
	B W	=	a rating value relating to the credibility of primary losses a rating value which relates the credibility of excess losses to the credibility of primary losses

The rating values, B and W, vary by size of risk as measured by Expected Total Loss, E.1

Actual Primary Losses, Ap, are determined by applying the following formula to each loss:

(2) 
$$Primary Loss = \frac{9,000 \times Actual Total Los}{Actual Total Loss+7,000}$$

This formula is known colloquially as the "split formula." All losses less than or equal to \$2,000 are wholly primary.

Though not immediately obvious, it can be shown that this modification formula defines implicitly primary and excess credibilities in terms of the rating values by the following relationships:

(3) Primary Credibility, 
$$Zp = \frac{E}{E+B}$$

(4) Excess Credibility, 
$$Ze = W \times Zp = \frac{W \times E}{E+B}$$
 Note that  $W = \frac{Ze}{Zp}$ 

Where, primary credibility is the credibility attaching to primary losses (Ap); excess credibility, the credibility attaching to excess losses (Ae). Again, for the purposes of this analysis, we accept

<sup>&</sup>lt;sup>1</sup>This paper presumes the reader is knowledgeable about workers compensation experience rating. The reader requiring additional background should consult the experience rating readings in the Casualty Actuarial Society's *Syllabus of Examinations*. In particular, see Gillam and Snader [1], Venter [2], and Gillam [3].

these credibility formulas as given. We do not consider whether other experience rating designs (such as a frequency-only plan, a frequency/severity split, or credibilities based on variables other than expected loss) might exist which are more accurate. Similarly, the split formula has not been reviewed to determine whether or not it is optimal.

#### Overview of the Methodology

Our goal is to determine, simultaneously, the primary and excess credibilities (Zp and Ze) appropriate for a risk of a given size. We will then translate our estimates of Zp and Ze into B and W rating values using Formulas 3 and 4. We cannot estimate Zp and Ze directly from the experience rating formula (Formula 1). However, after a little algebra, Formula 1 can be expressed as:

(5) Modification = 1 + 
$$Zp \frac{Ap-Ep}{E}$$
 +  $Ze \frac{Ae-Ee}{E}$ 

where, to parameterize, we let Modification equal the *projection period empirical modification* or Actual Total Losses/Expected Total Losses for the projection period. Modification is the dependent variable in our model. The algebraic conversion of Formula 5 into Formula 1 is given in Appendix 1.

The actual and expected losses on the right hand side of the equation are for the *experience period*. We term [(Ap-Ep)/E] and [(Ae-Ee)/E] the *primary variable* and *excess variable*, respectively. The primary and excess variables are empirical values and are the independent variables in our model. Zp and Ze are the regression parameters to be estimated on these independent variables. As a practical matter, we will not estimate these parameters on an individual risk basis but rather by groupings, based on size and experience. Before continuing with the methods used to estimate Zp and Ze, we will discuss the construction of the database and the development of the groupings.

## 2. THE DATABASE

We will demonstrate the methodology by parameterizing the policy year 1991 at fifth report projection period. The experience period for policy year 1991 modifications is policy year 1987 at third report, 1988 at second report, and 1989 at first report, combined. For each risk, the following data was compiled:

Experience Period (three policy years combined) Exposure (generally, reported subject payroll) Expected Total Losses (based on Expected Loss Rates by class for the experience period) Expected Primary Losses (based on empirical D Ratios, discussed below) Expected Excess Losses (Expected Total Losses - Expected Primary Losses) Actual Total Losses (subject to \$175,000 per claim loss limit; \$350,000 per catastrophe)

Actual Primary Losses (based on the split formula discussed above) Actual Excess Losses (Actual Total Losses - Actual Primary Losses)

<u>Projection Period (one year)</u> Exposure (generally, reported subject payroll) Actual Total Losses (subject to \$175,000 per claim loss limit; \$350,000 per catastrophe) Expected Total Losses (based on Expected Loss Rates by class for the projection period)

The empirical Expected Loss Rates (ELRs) are developed from the actual experience for the experience period (i.e., they are hindsight). Therefore, there is no systematic bias in the parameterization due to estimation error of the ELRs. Similarly, empirical D Ratios were determined using the policy year 1991 experience period data and the appropriate experience rating loss limit and death values. In practice, promulgated ELRs and D Ratios are estimated as all of the experience period data will not be collected until the experience modification for the last risk for a given projection period is issued. The empirical D Ratios tie to the actual experience and therefore parameter bias is again eliminated by benefit of hindsight. Because empirical ELRs and D Ratios are used, a risk's modification as calculated for this analysis is not necessarily the same as the modification actually promulgated for the policy year 1991 projection period. Appendix 2 provides the complete table of empirical ELRs and D Ratios for the policy year 1991 experience period. Appendix 3 provides a comparison of the empirical D Ratios in Appendix 2 with the D Ratios in the 1991 Experience Rating Manual for 39 "benchmark classes."

#### Partitioning of the Dataset and Grouping of Risks

There is a great deal of variation in the experience of individual risks. Later in this paper we will compare the performance of experience rating alternatives by looking at a measure of the proportionate reduction in total variance achieved by experience rating alternatives. To the uninitiated, the achieved reductions in variance which we will see, particularly for small risks, may seem surprisingly small. The variation explained by experience rating may be only about 1% for risks near the eligibility threshold. Yet this marginal improvement in pricing is just as important to the bottom line in insurance as the small marginal profit (typically less than 3%) of a grocery store's is to its bottom line. The variation explained for the largest risks is generally in excess of 15%.

But here we address the implications of individual risk variance to the organization of the data. Although attempts were made to avoid grouping risks, thereby retaining as much individual information as possible. there was too much variation in the individual risks' experience to obtain statistically reliable results using regression techniques.

This is not to say results could not be obtained--they were. But it was critical that we be able to statistically evaluate the results. For example, we needed reliable answers to questions such as: 'Does a shifted-logistic fit better than a regular logistic or some other curve?' and 'Is the bias in a plan, as measured by a weighted regression, statistically significant?' Because it is so large, the

unexplained individual risk variation often overwhelmed the tests of statistical significance. To overcome this, risks were first partitioned into groups of similar size and then further sub-grouped based on their experience. Many partitioning and grouping schemes were explored with the mean results of each more or less the same. We decided on the following scheme which we found to be optimal for statistical significance.

First, all risks were sorted by experience period Expected Total Losses in descending order. The risk with the largest Expected Total Losses in the database is risk "number one." The risks were then partitioned into groups of 5,000. The five thousand largest risks made up group 1-5,000, or the "first group." Within each group of 5,000, risks were then sorted based on their experience period empirical modifications (experience period Actual Total Losses/Expected Total Losses) in ascending order. Claim-free risks, if any, would be among the first of each group of 5,000. When risks had the same experience period empirical modification (commonly for claim-free risks), they were sorted by experience period Expected Total Losses in descending order. Therefore, the first risk in a group of 5,000 where there was more than one risk with claim-free experience would be the largest risk with claim-free experience.

Within each group of 5,000, sorted as described above, the risks were divided into 100 sub-groups of 50 risks. The experience of each sub-group of 50 risks was combined (not averaged) to make one data record. Then, for each group of 5,000, ridge regression (discussed below) was performed on the 100 (5,000 / 50) data records.

## The First Group--The Largest 5,000 Risks

The largest 5,000 risks form a more heterogeneous group in terms of size than any other group. For example, the average expected loss for the larger half of the first group, \$1,633,606, is 4.2 times larger than for the smaller half, while the average expected loss for the larger half of the second group, \$248,855, is 1.4 times larger than for its smaller half. Because of this, consideration was given to breaking up the largest 5,000 into five groups of a thousand. No significant improvements or meaningful differences in estimates resulted from this refinement. Further, breaking the first group into smaller groups would have necessitated the use of weighted regressions, complicating the analysis. Therefore, we chose to leave the largest risks in one group of 5,000.

We now return to directly estimating Zp and Ze, simultaneously, from Formula (5).

## 3. PARAMETERIZING THE PLAN

## Multicollinearity and the Primary and Excess Variables

Unfortunately, we cannot apply straightforward multivariate regression because the primary and excess variables are highly correlated. This is not unexpected given the nature of the split

formula. For example, for the first group of 5,000 the correlation between the primary and excess variables is 99.0% for the policy year 1991 experience period. For the sixth group, (risks 25,001 - 30,000) the correlation is 96.3%. This high degree of multicollinearity can result in unstable parameters of uncertain statistical reliability.

Is the multicollinearity present in the data severe enough to warrant an alternative estimation procedure? We will see later that it certainly is.

We explored several possible solutions to this problem and ultimately decided on ridge regression as the appropriate treatment. While ridge regression is commonly used in other disciplines, it is currently not covered in the Casualty Actuarial Society's *Syllabus of Examinations*, so many actuaries may be unfamiliar with it. Therefore, we provide here an introduction and, for the interested reader, further references. But first, we will briefly sketch the steps to follow so the reader will have context for the role of ridge regression in our overall methodology.

The ridge regression estimates are starting values in an iterative process. At each iteration we will refine *overall* credibilities using an extension of the traditional quintile tests used to evaluate experience rating plan performance and then refer back to the ridge regression results to determine appropriate *apportionments* between primary and excess credibilities. Each iteration will involve translating primary and excess credibilities into B and W rating values and recalculating modifications for each risk. This iterative process will continue until no further improvements in plan performance can be obtained by adjusting primary and excess credibilities.

## Ridge Regression Overview

Ridge regression introduces a parameter,  $\theta$ , into the least squares solution.<sup>2</sup> The vector of parameter estimates is given by the equation:

$$\mathbf{b}_{\mathbf{z}}(\theta) = (\mathbf{Z}^{*}\mathbf{Z} + \theta I_{p})^{\cdot \mathbf{I}}\mathbf{Z}^{*}\mathbf{Y}$$

where Z is the vector of predictor variables, Ip is the identity matrix of dimension p, and Y is the vector of centered and scaled empirical modifications. When  $\theta$  equals zero, the ridge regression estimates are the same as the usual least squares estimates. Exhibit 1 provides the ridge regression results for three select groups of 5,000 for the policy year 1991 projection year.

The ridge regression results, or ridge trace, on Exhibit 1 demonstrate that for ordinary least squares--that is, when  $\theta$  equals zero--the estimates of primary credibility were generally greater than one, while the estimates of excess credibility were very small or even negative. For example, on Exhibit 1, multivariate regression for the fifth group gives Zp of 1.5959 and Ze of -0.0368. Clearly, these results violate our *a priori* constraints for the values of Zp and Ze--namely that Zp

<sup>&</sup>lt;sup>2</sup>The following discussion of ridge regression summarizes the key points from our primary reference, Draper and Smith [4]. The reader may also find Miller and Wichern [5] and Johnson and Wichern [6] helpful.

and Ze are bounded by [0,1]. The ordinary least squares results shown in Exhibit 1 are typical for all sizes groups and partitioning schemes.

The introduction of a  $\theta$  greater than zero in the equation for the parameter vector above can correct for the correlation between the variables, the cause of these unacceptable results. The parameters of the resulting equations are not least squares and are biased, but are more stable and, generally, of smaller mean square error. The stability and lower variance error should more than compensate for the bias introduced.<sup>3</sup>

Exhibit 2 provides a plot of each group's ridge trace, that is, a graph of  $\theta$ , Zp and Ze from Exhibit 1. Determining the appropriate degree of correction--the appropriate  $\theta$ --is key. As  $\theta$  goes to infinity, the parameters will approach zero. The goal is to keep  $\theta$  as small as possible to achieve the desired degree of correction. There are many approaches to selecting the optimal  $\theta$ , which we will designate by  $\theta^*$ . Draper and Smith [4] state that there is no mechanically best way to choose  $\theta^*$ . We experimented with most of the methods discussed by Draper and Smith.<sup>4</sup> Ultimately, we developed our own method, the Maximum Excess method, which outperformed the other methods we tested.<sup>5</sup>

The Maximum Excess method begins by inspecting the ridge trace to locate that  $\theta$  for which excess credibility is maximized, subject to the constraint that Zp and Ze are bounded by [0,1]. An examination of Exhibit 2 reveals that, for each group, there is a  $\theta$  for which excess credibility is maximized. We term this  $\theta$  our *maximum excess*  $\theta$ ,  $\theta_E$ . We select the combination of primary and excess credibilities corresponding to  $\theta_E$  for our initial credibility estimates. For example, on Exhibit 1, excess credibility is maximized when  $\theta$  equals 0.27 for the fifth group. Therefore,  $\theta_E =$ 0.27 and we select Zp = 0.7186 and Ze = 0.1273 as initial values for the fifth group. This process is repeated for each group. Exhibit 3 provides a summary of each group's Maximum Excess selections. The corresponding values promulgated in the 1997 Plan are also shown for comparison. Note that, because this is empirical data, the Maximum Excess credibilities are not monotonically decreasing across groups. The Fitted Credibilities on Exhibit 3 smooth out this empirical noise. We'll come back to the Fitted Credibilities shortly, but first, a few more comments on ridge regression.

<sup>&</sup>lt;sup>3</sup>Tests performed while developing the 1997 Plan parameters found that the methodology in this paper developed *overall* credibilities comparable to those obtained with the prior methodology which was last used to parameterize the 1984 Plan and which did not correct for multicollinearity. The prior methodology did not allow for direct estimation of primary and excess credibilities separately nor for the ability to directly translate these credibilities into B and W rating values.

<sup>&</sup>lt;sup>4</sup>An overview of the most promising method discussed by Draper and Smith, Hoerl and Kennard's  $\delta$ , is provided in Appendix 4.

<sup>&</sup>lt;sup>5</sup>In prior analyses, the Maximum Excess method resulted in the best parameters, as indicated by our performance measures (discussed below), see Workers' Compensation Insurance Rating Bureau of California [7], [8], and [9]. A comparison of the relative performance of the Hoerl and Kennard's  $\delta$  method with that of the Maximum Excess method is provided in the Agenda and Minutes of the July 2, 1996 Meeting of the Actuarial Committee of the Workers' Compensation Insurance Rating Bureau of California [8].

The ordinary least squares estimates of Zp and Ze routinely fall outside the [0,1] constraint thus demonstrating the need to address multicollinearity. We have selected ridge regression as the treatment. As to ridge regression's appropriateness, we note here that Draper and Smith [4] discuss two circumstances for which ridge regression is "absolutely" the correct way to proceed. The first is when we have "[a] Bayesian formulation of a regression problem with specific prior knowledge of a certain type on the parameters." The second is when we have "[a] formulation of a regression problem as one of least squares subject to a specific type of restriction on the parameters." The constraint on credibilities to be between zero and unity justify ridge regression in this situation. Indeed, it may be possible to further refine the ridge regression procedure to the *a priori* constraints (for example, the parameters could be constrained to the ellipse 0 <= Ze <= Zp <= 1).

Miller and Wichern [5] discuss several ways to deal with the problems of multicollinearity, including reselection of the independent variables, discarding independent variables, alternative estimation procedures and ridge regression. Clearly, discarding a variable is not an option here. A principal components treatment would be feasible but would require altering the familiar B and W structure of the rating plan as there would be no simple, direct linkage (i.e., Formulas 3 and 4) between primary and excess credibilities and the B and W rating values.

## Smoothing the Primary and Excess Credibilities

The ridge regressions have given us a series of indicated primary and excess credibilities by size of risk. We test each iteration's credibilities by calculating experience modifications for every eligible risk. The Bureau's systems are designed to accommodate Formula (1), the traditional B and W formula. To accomplish this mass re-rating requires development of a B and W table for each iteration. To develop a B and W table we first smooth the selected credibilities by fitting them to a curve.

The series of credibilities corresponding to the selected  $\theta$ s is smoothed by fitting the primary series and excess series separately, to a logistic cumulative density function (CDF). The logistic CDF is given by

$$F(x) = \frac{1}{1 + \exp[(\alpha - X)/\beta]}$$

where X = the natural logarithm of a group's median Expected Total Losses for the experience period. Excess credibilities were fit to a translated, or shifted, logistic CDF, where

$$F(x) = \frac{1}{1 + \exp[(\alpha - X)/\beta]} - \text{Shift}$$

A statistically significant shift greater than zero implies that excess credibility approaches a limit less than one (specifically, unity minus the shift). The credibilities were fit by applying the nonlinear Levenberg-Marquardt algorithm to the indicated ridge regression Zp and Ze. Exhibit 4

shows the indicated and fitted values for the initial iteration. Finally, we note that, for the B and W table to have the usual properties of B descending and W ascending with increasing Expected Total Loss, the parameter  $\beta$  must be less than unity for primary credibility.

#### Developing B & W Rating Values from the Primary and Excess Credibilities

Exhibit 5 provides the formulas used to translate the fitted primary and excess credibility curves to B and W values. First, the fitted equations for Zp and Ze are shown. We then make use of the fact that W = Ze/Zp. Using some straightforward (though unattractive) algebra, we can express W in terms of the natural logarithm of the experience period Expected Total Losses, E. With this closed form expression for W, we can determine the Expected Total Losses corresponding to any given W. (Theoretically, we could do this by inverting the equation; practically, we do this using Lotus 1-2-3's Backsolver or a bi-section algorithm.)

We construct the Table of B and W values (Exhibit 6) by first determining the Total Expected Loss ranges for each W in increments of 0.01. For example, to determine the Expected Loss range corresponding to W = 0.25, we determine (using Exhibit 5, Formula 3 and Lotus 1-2-3's Backsolver) the expected losses corresponding to W = 0.245 and W = 0.255. Next, we determine the Total Expected Losses corresponding to the midpoint of each range by averaging the endpoints (\$215,673 for W = 0.25). For the midpoint Total Expected Losses we determine Zp (Exhibit 5, Formula 1). Finally, we use Formula 4 of Exhibit 5, which is a closed form expression for B in terms of E and Zp, to determine B for the midpoint of each Expected Loss Range.

#### Iterative Parameter Refinement

A number of tests were used to assess the performance of each set of credibilities. Each test was performed for all risks and for five groups of risks based on size (Expected Loss Quintiles).

Quintile tests were examined to assess the overall performance of parameters. A quintiles test first ranks risks by their experience modifications, then divides the population into five groups (quintiles), and then compares their relative standard and manual loss ratios. Each modification quintile has approximately 20,000 risks. Quintiles tests are a commonly accepted actuarial technique for evaluating the performance of experience rating plans [2]. The quintiles tests are shown in Exhibit 7. Ideally, we expect the standard loss ratios (the loss ratios using the modified premiums) for all groups to be the same. If a group's standard loss ratio is markedly higher or lower than the others, this indicates that the general credibility for the group is too low or too high. In particular, there should be no marked trend in the standard loss ratios and we would like the variance of the standard loss ratios to be small. Conversely, we expect the manual loss ratios to be positively correlated with the experience modifications. This indicates the experience modification does a good job of differentiating risks based on their expected future experience. If the plan did not do this, the manual loss ratios would tend to be the same.

We developed an extension of the quintiles test in which we regress the standard loss ratio against the experience modification. Exhibit 8 shows the standard loss ratios and number of risks by intervals of the projected experience modification for five groups based on size and for all risks combined. Again, absent noisy data, a perfect plan would produce the same loss ratio after modification for all risks. To determine what adjustments, if any, might be necessary, we look for patterns in the standard loss ratios across modification interval for risks of approximately the same size (a given Expected Loss Quintile). We quantify the pattern by performing a weighted regression. Generally, the pattern, if any, is a simple trend and we fit this with a straight line. The coefficient on the independent variable (projection modification) quantifies how much credibility should be increased or decreased. If all risks' standard loss ratios are the same, the coefficient will not be significantly different (statistically) from zero and no adjustment is indicated. If standard loss ratios are positively correlated with the proposed modifications, then credibilities are too low. If standard loss ratios are negatively correlated with the proposed modifications, then credibilities are too high. (The logic behind this adjustment is presented in Appendix 5.) The R-squared for the regression as a whole relates to the amount of variation explained and generally is expected to be small for experience rating. The statistical significance of the coefficient on the independent variable, the indicated adjustment, generally is significant at a 5% or 10% confidence level. When this coefficient is statistically insignificant, we exercise judgment in making an adjustment. The results of these regressions are provided in Exhibit 9.

The quintile test weighted regressions indicate that the appropriate adjustments to credibility vary by size. For example, from Exhibit 9 we see that the indicated adjustment for the largest risks is 0.04859 while for the smallest risks it is 0.3835. To account for this variation by size, the indicated adjustments (the coefficients on the independent variable) for each size quintile are fit to the quintiles' median risk ranks to determine a smooth transition in adjustment by size (Exhibit 10). When the pattern of adjustments is not smooth across size quintiles, linear interpolation from quintile to quintile may be used. Exhibit 11 provides a plot of the bias adjustments for the initial and subsequent iterations. As our estimates are refined, we expect the line graphed on Exhibit 11 to fall toward the x-axis with successive iterations, assuming the bias coefficients maintain their statistical significance.

From this fit of indicated adjustments to size of risk, an adjustment appropriate to each group of 5,000 can be calculated. The indicated adjustment for each group is then applied to the *overall* credibility underlying the prior iteration to determine the Overall Credibility After Adjustment (Exhibit 12).

Our new overall credibilities for the next iteration must now be split into primary and excess components. The problem for successive iterations is how to select primary and excess credibilities which are not highly multicollinear. To clarify our chosen solution to this problem, let us first consider a theoretically more idealistic solution. We propose that for each group, some combination of Zp and Ze on the ridge trace is optimal in terms of optimizing a given performance measure as well as correcting for multicollinearity. Specifically, given any performance measure, we could determine each group's optimal  $\theta$  by developing a B and W table for each valid Zp/Ze combination on the ridge trace (i.e., for each  $\theta$  for which Zp and Ze are bounded by [0,1]),

calculate the corresponding performance measure and select the optimal combination. These results could then be smoothed out across risk sizes as discussed above.

Such a method, while theoretically appealing, is currently too computationally intensive. The Maximum Excess method, logistic smoothing, and quintile adjustments serve to get us reasonably close. Because the goal is more optimal positioning on the ridge trace for each group--not proportionate adjustment--we return to the ridge trace to find Zp and Ze combinations for which the overall credibility is closest to the new indicated credibility.

An example will clarify our procedure. For the fifth group, the overall fitted credibility before adjustment was 0.2931 (Exhibit 12). The indicated adjustment for this group from Exhibit 10 is to increase credibility 12.76%. So the desired overall credibility after adjustment is 0.3306. Returning to the ridge trace for this group, Exhibit 1, we find the Zp and Ze which provide overall credibility closest to 0.3306 at  $\theta = 0.11$ . Our credibility selections for the fifth group to start the first iteration become Zp = 0.8662 and Ze = 0.1155. (The initial Maximum Excess values were lteration 0.) This procedure is followed for each group. For each iteration credibilities are then logistically smoothed before preparing the B and W table.<sup>6</sup>

The above process is repeated iteratively until a set of credibilities is developed for which the overall performance of the plan was maximized and no further adjustments to credibility were indicated. Generally, we determine this point by going too far. That is, adjusting until the performance deteriorates and then selecting the prior iteration.

#### 4. EVALUATING THE PARAMETERIZATION

#### The Performance Measure

The selected performance measure is the efficiency of each iteration; that is, the proportionate reduction in total variance. This measure was developed by Meyers [10]. We have calculated each tested plan's efficiency on both a manual premium-weighted and risk-weighted basis and by size quintile and for all risks combined. The manual-premium basis attaches weights so as to minimize error in terms of absolute dollars. The risk-weighted basis implies the accuracy of a small 10-employee risk is of the same importance in parameter development as a large 10,000-employee risk. While generally not true, there is concern that the risks who must live with their experience modifications without recourse are smaller risks. Large risks are more likely to receive special scrutiny and have options largely unavailable to small risks, such as retrospective rating, large deductible plans, or schedule rating. Therefore, when looking at the all risks

<sup>&</sup>lt;sup>6</sup>Other approaches were considered but dismissed. For example, a straightforward approach might be to increase both Zp and Ze by the indicated adjustment, allowing for special handling when the indicated primary credibility would be in excess of unity. This approach was tried in the early stages of our research but the results proved unsatisfactory and incongruous with the multicollinearity correction we sought through ridge regression. Another approach we considered was to maintain the relativity between primary and excess credibilities implied by the Maximum Excess selections. This approach's results also proved inferior.

combined efficiency, we look at both bases to ensure the best plan is not one which serves only one class of risks.

Exhibit 13 summarizes the efficiencies of each iteration. The credibilities underlying the second iteration were selected as final since no further improvements in the all risks, manual premium-weighted efficiency were achieved after this iteration. For reference, risk-weighted efficiencies are shown for the promulgated 1997 Plan and a frequency-only plan developed in 1995.<sup>7</sup> The promulgated 1997 Plan's credibilities were based on parameterizing the policy year 1989 projection period as well as looking at other projection periods. The frequency-only plan was developed in 1996 as an alternative to the existing experience rating formula. In the end, the frequency-only plan was not adopted. However, the efficiencies for the frequency-only plan suggest that most of the information from the current experience rating formula comes from frequency.

We note that great care must be made in comparing efficiencies across projection periods. Experience rating works best when the same dynamics extend from the experience period through the projection period. Some periods in time are more or less stable than others. In California, in particular, highly aberrant and extreme experience was observed for policy years 1989 through 1991. Generally, the Bureau tries to avoid using these years in studies such as this, but tradeoffs must be made between the availability and age of data.

We also note that our experience in California suggests parameterizing an experience rating plan is less sensitive to the maturity of the data than might be first thought.<sup>\*</sup> This is probably true for several reasons. First, under the current formulation, frequency accounts for most of the variation explained by experience rating. Second, the severity of individual claims is limited. So, using loss limitations effective for policy year 1998 ratings, of a claim which develops from \$50,000 to \$500,000, only an additional \$125,000 would be allowed in the experience rating. And finally, of the incremental dollars which would enter the experience rating, virtually all would be excess and subject to excess credibilities (around 33% for the largest risks and less than 10% for most risks). Indeed, the proportion of losses which are primary has grown substantially since the current split formula was last updated in 1985 (Appendix 6). The \$175,000 loss limitation has also been in effect since 1985.

#### Impact Tests

Finally, we examine the distribution of risks by current vs. indicated modifications, separately by Expected Loss Quintile and for all risks combined. This information, for the second and final iteration, is shown in Exhibit 14, and provides an overview of the number of risks which will be impacted in any given direction and the magnitude of the impact. The shaded diagonal on Exhibit 14 marks those risks with no appreciable change in modification. The further a risk is away from

<sup>&</sup>lt;sup>8</sup>The reader might note that the policy year 1989 parameterizations were to third report level data while the policy year 1991 parameterizations are to fifth report level data.



<sup>&</sup>lt;sup>7</sup>Manual premium-weighted efficiencies were not available.

the diagonal, the larger the impact of the revision in credibilities. Risks above the diagonal would see their modifications go down. Risks below the diagonal would see their modifications go up.<sup>9</sup> While the information presented in Exhibit 14 is in 0.10 increments, the Bureau reviews the impact tests in 0.01 increments in making its final evaluation. This information, in light of this analysis and findings in prior analyses, is used in any decisions to deviate from the indicated credibilities.

Exhibit 15 provides a comparison of indicated and promulgated credibilities for the 1997 Plan and the indicated credibilities for the policy year 1991 parameterization.<sup>10</sup> Exhibit 16 is a graphical presentation of the information on Exhibit 15. Exhibit 17 provides a comparison of indicated and promulgated B and W values for the 1997 Plan and the indicated B and W values for the policy year 1991 parameterization. Exhibit 18 is the graphical companion to Exhibit 17.

## 5. DISCUSSION AND CONCLUSION

In 1998, the Bureau's Actuarial Committee reviewed the analysis presented above and decided to make no changes to credibilities at that time. Instead, the Bureau's Actuarial and Governing Committees directed further research which will follow from the following discussion. The procedures demonstrated, however, are the same as those used to develop the credibilities underlying the experience rating plan current as of this writing (namely, for policies effective in 1997 through 1999)

The credibilities developed for policy year 1991 are quite different from those developed for policy year 1989 and earlier periods. In particular, primary credibilities are much higher across all risk sizes while excess credibilities are somewhat lower (Exhibit 17). We noted earlier that the proportion of loss dollars which are primary has grown considerably since the split formula was last updated (Appendix 6). We expect this explains much of this shift in credibilities. This shift was probably evident in 1989, but that was a period characterized by many small stress claims from plant closings and fraudulent claims from 'medical mills,' for example, which masked the shift at that time. The evidence argued for a review of the split formula and it was decided this would be done before revising the Plan credibilities.

The split formula can be thought of as one point in a spectrum between a frequency-only plan, where primary losses are limited to one dollar and all excess credibilities are zero, and self-rating,

<sup>&</sup>lt;sup>9</sup>Because revising credibilities will likely change a plan's off-balance, risks with no change to their modification may actually see a modest change in standard premium. Similarly, risks with modest changes in modification may even see their standard premium change the slightly in the opposite direction.

<sup>&</sup>lt;sup>10</sup>The credibilities indicated for the 1997 California Experience Rating Plan were not adopted for all sizes of risks. The Bureau's Actuarial Committee elected to phase-in indicated credibilities for smaller risks. This was accomplished by allowing no change for the smallest risks for which B and W values were published and allowing the full change for risks with experience period expected losses of \$20,000 or greater. To prevent a misleading comparison between the 1997 Plan and projection year 1991, Exhibits 15 through 18 show both the indicated and promulgated values for the 1997 Plan.

where full credibility attaches to both frequency and severity.<sup>11</sup> We noted that frequency-only alternatives have been developed which explain nearly as much variation as the current plan. This suggests a frequency/severity split might offer even greater performance. For our future research we propose to first isolate the predictive content of frequency experience and then to examine the predictive power of layers of severity. Such an approach might obviate the need to address multicollinearity.

We continue to work on other avenues to improve our methodology. For the quintiles test extension and bias adjustments of Exhibits 9 and 10, we are exploring refinement of the adjustments to the group-of-5,000 level, perhaps even adjusting each group independently to its optimal credibilities then smoothing across size of risk.

As with any project of this scale, of course, honing our methodology will always be a work in progress. To date, we have had neither the time nor resources to explore all the paths which might lead to further improvement. Nevertheless, this latest methodology has proved very satisfactory since its development and has offered new insights into the dynamics of experience rating.

<sup>&</sup>lt;sup>11</sup>It happens that the frequency-only alternative we developed treated types of claims differently. Specifically, temporary and other indemnity claims were treated separately and medical-only frequency was not used at all. This does not detract from the proposed spectrum, but it does increase its complexity.

<sup>343</sup> 

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# CALIFORNIA EXPERIENCE RATING PLAN RIDGE REGRESSION RESULTS Projection Year 1991 5th Report

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Risks 1	- 5,000 (1s	t Group)	]	Risks 20,0	01 - 25,000 (	5th Group)	Risks 45,0	01 - 50,000 (	10th Group)
0.00         1.8494         0.0790         0.6388         1.5959         -0.0368         0.4330         1.1171         -0.0131         0.2079           0.01         1.4293         0.2210         0.6630         1.3700         0.0142         0.3865         0.9902         0.0119         0.2898           0.03         1.2188         0.2869         0.5815         1.1246         0.0642         0.3865         0.9902         0.0179         0.2829           0.04         1.1431         0.3052         0.5708         1.0263         0.0776         0.3550         0.0300         0.22719           0.05         1.1195         0.3190         0.5566         0.9951         0.3517         0.8432         0.0390         0.2674           0.07         1.1066         0.3141         0.5528         0.9540         0.1013         0.3466         0.8181         0.0433         0.2674           0.09         1.0144         0.3175         0.5529         0.9269         0.1060         0.3183         0.7761         0.0501         0.2563           0.11         1.0489         0.3187         0.5437         0.8365         0.1177         0.3285         0.7138         0.0573         0.22643           0.121	θ	Zp	Ze	Overall		Zp	Zc	Overall	Zp	Ze	Overall
0.01         1.4293         0.2210         0.6030         1.3700         0.0142         0.4043         1.0467         0.0099         0.2979           0.03         1.2188         0.2869         0.5815         1.1426         0.0442         0.3856         0.9002         0.0119         0.2898           0.03         1.2188         0.2869         0.5815         1.0765         0.0776         0.3650         0.9020         0.0219         0.2770           0.05         1.1416         0.05666         0.9865         0.0877         0.8719         0.0339         0.2674           0.07         1.1006         0.3141         0.5528         0.9269         0.1060         0.3422         0.7959         0.0469         0.2597           0.09         1.0714         0.3175         0.5559         0.9038         0.1099         0.3383         0.7761         0.0501         0.2532           0.12         1.0489         0.3187         0.5496         0.8862         0.1135         0.3348         0.7383         0.2524           0.12         1.0333         0.3187         0.5496         0.8862         0.1135         0.3148         0.7383         0.2524           0.11         1.0480         0.3180	0.00	1.8494	0.0790	0.6388		1.5959	-0.0368	0.4330	1.1171	-0.0131	0.3079
0.02         1.2901         0.2657         0.5896         1.2140         0.0442         0.3865         0.9902         0.0119         0.2839           0.04         1.1743         0.2886         0.5815         1.1075         0.0638         0.3517         0.8439         0.0207         0.2829           0.05         1.1431         0.3052         0.5708         1.0263         0.0877         0.3517         0.8412         0.0390         0.2674           0.06         1.1195         0.3109         0.5566         0.9950         0.0160         0.3142         0.7599         0.0469         0.2597           0.07         1.1066         0.3183         0.5527         0.9838         0.1130         0.3466         0.8528         0.7761         0.0529         0.2597           0.09         1.0714         0.3187         0.5437         0.8838         0.1130         0.3348         0.7563         0.0529         0.2421           0.10         1.0546         0.3187         0.5446         0.8806         0.1177         0.3285         0.7138         0.0573         0.2242           0.14         1.0221         0.3180         0.5466         0.88121         0.1222         0.3285         0.7138         0.0590 <td>0.01</td> <td>1.4293</td> <td>0.2210</td> <td>0.6030</td> <td>L</td> <td>1.3700</td> <td>0.0142</td> <td>0.4043</td> <td>1.0467</td> <td>0.0009</td> <td>0.2979</td>	0.01	1.4293	0.2210	0.6030	L	1.3700	0.0142	0.4043	1.0467	0.0009	0.2979
0.03         1.2188         0.2869         0.5815         1.1426         0.0638         0.3742         0.9439         0.0207         0.2829           0.05         1.1431         0.3062         0.5708         1.0263         0.0877         0.35577         0.8419         0.0379         0.2779           0.06         1.1195         0.3109         0.5666         0.9865         0.0951         0.3517         0.8412         0.0390         0.2674           0.07         1.1006         0.3141         0.5528         0.9269         0.1060         0.3462         0.0510         0.2553           0.09         1.0714         0.3137         0.5496         0.8662         0.1155         0.3318         0.7583         0.0529         0.2353           0.11         1.0489         0.3183         0.5466         0.8506         0.1177         0.3285         0.7123         0.0574         0.2471           0.13         1.0304         0.3188         0.5466         0.8506         0.1174         0.3285         0.7134         0.0593         0.2428           0.14         1.0221         0.3184         0.5409         0.8237         0.1232         0.3185         0.5462         0.2428           0.143	0.02	1.2901	0.2657	0.5896	L	1.2340	0.0442	0.3865	0.9902	0.0119	0.2898
0.04         1.1743         0.2988         0.5756         1.0765         0.0776         0.3577         0.9050         0.0279         0.2770           0.05         1.1195         0.3109         0.5578         1.0263         0.0877         0.3577         0.8719         0.0339         0.2719           0.06         1.1195         0.3109         0.5568         0.9960         0.0131         0.3466         0.8181         0.0433         0.2674           0.07         1.006         0.3141         0.5529         0.9269         0.0100         0.3422         0.7959         0.0460         0.2597           0.09         1.0714         0.3183         0.5527         0.8388         0.1130         0.3348         0.7761         0.0529         0.25332           0.10         1.0499         0.3188         0.5466         0.8662         0.1157         0.3258         0.7713         0.0574         0.2477           0.13         1.0304         0.3184         0.5466         0.8662         0.1157         0.3258         0.7713         0.3258         0.7138         0.0579         0.2424           0.141         1.0221         0.3184         0.5491         0.1224         0.3183         0.6789         0.0624 <td>0.03</td> <td>1.2188</td> <td>0.2869</td> <td>0.5815</td> <td></td> <td>1.1426</td> <td>0.0638</td> <td>0.3742</td> <td>0.9439</td> <td>0.0207</td> <td>0.2829</td>	0.03	1.2188	0.2869	0.5815		1.1426	0.0638	0.3742	0.9439	0.0207	0.2829
0.05         1.1431         0.0362         0.5708         1.0263         0.0877         0.3577         0.8719         0.0339         0.2719           0.06         1.1195         0.3109         0.5666         0.9950         0.3517         0.8432         0.0390         0.2674           0.07         1.006         0.3141         0.5528         0.9269         0.1060         0.3422         0.7959         0.0469         0.2557           0.09         1.0714         0.3177         0.5575         0.9388         0.170         0.3348         0.7761         0.0529         0.2532           0.11         1.0489         0.3187         0.5496         0.8662         0.1155         0.3315         0.7421         0.0553         0.2254           0.12         1.0334         0.3184         0.5497         0.8237         0.1209         0.3231         0.7013         0.0610         0.2428           0.14         1.0221         0.3184         0.5497         0.8237         0.1209         0.321         0.7013         0.0610         0.2428           0.17         1.0000         0.3174         0.5354         0.8014         0.1222         0.3183         0.6789         0.06659         0.2345	0.04	1.1743	0.2988	0.5756	1	1.0765	0.0776	0.3650	0.9050	0.0279	0.2770
0.06         1.1195         0.3109         0.5666         0.9865         0.0531         0.3517         0.8422         0.0390         0.2674           0.07         1.1006         0.3141         0.5628         0.9540         0.1013         0.3466         0.8181         0.0433         0.2634           0.09         1.0714         0.3175         0.5559         0.9038         0.1099         0.3383         0.7761         0.0501         0.25563           0.10         1.0499         0.3187         0.5496         0.8662         0.1135         0.3348         0.7761         0.0574         0.22504           0.11         1.0499         0.3187         0.5496         0.8662         0.1155         0.3315         0.7721         0.0574         0.2250           0.13         1.0304         0.3187         0.5496         0.8306         0.1177         0.3258         0.7138         0.0610         0.2428           0.141         1.0221         0.3184         0.5409         0.8237         0.1229         0.3231         0.7138         0.0624         0.2406           0.161         1.0700         0.3174         0.5328         0.7914         0.1214         0.3161         0.6789         0.0642         0.2345	0.05	1.1431	0.3062	0.5708	1	1.0263	0.0877	0.3577	0.8719	0.0339	0.2719
0.07         1.1006         0.3141         0.5528         0.9540         0.1013         0.3466         0.8181         0.0433         0.2534           0.08         1.0849         0.3175         0.5559         0.9038         0.1099         0.3761         0.7761         0.0501         0.2563           0.10         1.0586         0.3187         0.5496         0.8838         0.1130         0.3348         0.7761         0.0501         0.2563           0.11         1.0489         0.3187         0.5496         0.8626         0.1155         0.7233         0.0574         0.2477           0.13         1.0304         0.3184         0.5409         0.8237         0.1220         0.3231         0.713         0.0610         0.2428           0.15         1.0143         0.3180         0.5328         0.7114         0.3180         0.6689         0.0624         0.2365           0.16         1.0070         0.3174         0.5328         0.7814         0.3139         0.6598         0.0649         0.2365           0.17         1.00000         0.3143         0.5250         0.7533         0.1244         0.3119         0.6505         0.2365           0.18         0.99850         0.3133	0.06	1.1195	0.3109	0.5666	1	0.9865	0.0953	0.3517	0.8432	0.0390	0.2674
0.08         1.0849         0.3162         0.5592         0.9269         0.1060         0.3422         0.7761         0.0469         0.2563           0.10         1.0596         0.3183         0.5527         0.8838         0.1130         0.3343         0.7761         0.0523         0.2563           0.11         1.0489         0.3187         0.5496         0.8662         0.1155         0.3315         0.7273         0.0573         0.2574           0.12         1.0393         0.3184         0.5437         0.8365         0.1194         0.3258         0.7138         0.0593         0.2452           0.14         1.0221         0.3184         0.5437         0.8365         0.1194         0.3258         0.7138         0.0593         0.2452           0.14         1.0210         0.3184         0.5437         0.8237         0.1229         0.3383         0.6789         0.06637         0.2385         0.7138         0.0593         0.2462         0.2406           0.16         1.0070         0.3143         0.5226         0.7735         0.1241         0.3116         0.6637         0.2345           0.17         0.9933         0.3134         0.5225         0.7756         0.1263         0.0342 <td>0.07</td> <td>1.1006</td> <td>0.3141</td> <td>0.5628</td> <td>L</td> <td>0.9540</td> <td>0.1013</td> <td>0.3466</td> <td>0.8181</td> <td>0.0433</td> <td>0.2634</td>	0.07	1.1006	0.3141	0.5628	L	0.9540	0.1013	0.3466	0.8181	0.0433	0.2634
0.09         1.0714         0.3175         0.5559         0.9038         0.1099         0.3383         0.7761         0.0501         0.2563           0.10         1.0596         0.3183         0.5527         0.8838         0.1130         0.3384         0.7583         0.0529         0.2532           0.11         1.0489         0.3187         0.5496         0.8662         0.1155         0.3315         0.7421         0.0553         0.2504           0.13         1.0304         0.3187         0.5437         0.8856         0.1144         0.3238         0.7138         0.0593         0.2452           0.14         1.0221         0.3184         0.5409         0.8237         0.1209         0.3231         0.7013         0.0610         0.2428           0.15         1.0143         0.3180         0.5381         0.8121         0.1222         0.3207         0.6689         0.0649         0.2365           0.16         1.0070         0.3143         0.5250         0.7653         0.1254         0.3119         0.6559         0.0669         0.2327           0.22         0.9690         0.3124         0.5250         0.7653         0.1259         0.3099         0.6421         0.0677         0.2309 <td>0.08</td> <td>1.0849</td> <td>0.3162</td> <td>0.5592</td> <td>L</td> <td>0.9269</td> <td>0.1060</td> <td>0.3422</td> <td>0.7959</td> <td>0.0469</td> <td>0.2597</td>	0.08	1.0849	0.3162	0.5592	L	0.9269	0.1060	0.3422	0.7959	0.0469	0.2597
0.10         1.0596         0.3183         0.5527         0.8838         0.1130         0.3348         0.7583         0.0529         0.2532           0.11         1.0489         0.3187         0.5496         0.8662         0.1155         0.3315         0.7421         0.0553         0.2504           0.12         1.0393         0.3188         0.5466         0.8506         0.1177         0.3258         0.7138         0.0593         0.2452           0.14         1.0211         0.3180         0.5381         0.8121         0.1222         0.3207         0.6897         0.0624         0.2462           0.16         1.0070         0.3174         0.5354         0.8014         0.1222         0.3183         0.6789         0.0637         0.2385           0.17         1.0000         0.3167         0.5328         0.7735         0.1264         0.3119         0.6504         0.06699         0.2345           0.19         0.9867         0.3143         0.5225         0.7576         0.1263         0.3079         0.6421         0.6677         0.2309           0.221         0.9690         0.3125         0.5176         0.7245         0.3277         0.3007         0.6641         0.6777         0.2275 </td <td>0.09</td> <td>1.0714</td> <td>0.3175</td> <td>0.5559</td> <td></td> <td>0.9038</td> <td>0.1099</td> <td>0.3383</td> <td>0.7761</td> <td>0.0501</td> <td>0.2563</td>	0.09	1.0714	0.3175	0.5559		0.9038	0.1099	0.3383	0.7761	0.0501	0.2563
0.11         1.0489         0.3187         0.5496         0.8662         0.1155         0.3315         0.7421         0.0533         0.2504           0.12         1.0393         0.3188         0.5466         0.8506         0.1177         0.3285         0.7731         0.0573         0.2477           0.13         1.0304         0.3187         0.5437         0.8365         0.1194         0.3285         0.7138         0.0593         0.2442           0.15         1.0143         0.3180         0.5381         0.8121         0.1222         0.3187         0.5464         0.2428           0.16         1.0070         0.3174         0.5354         0.8014         0.1232         0.3161         0.6629         0.2465           0.18         0.9933         0.3160         0.5302         0.7822         0.1248         0.3199         0.66421         0.06677         0.2305           0.19         0.9869         0.3125         0.5276         0.7735         0.1254         0.3119         0.6505         0.06659         0.2217           0.22         0.9670         0.3125         0.5276         0.7734         0.1268         0.3042         0.6194         0.06977         0.2239           0.21	0.10	1.0596	0.3183	0.5527		0.8838	0.1130	0.3348	0.7583	0.0529	0.2532
0.12         1.0393         0.3188         0.5466         0.8506         0.1177         0.3285         0.7733         0.0574         0.2477           0.13         1.0304         0.3187         0.5437         0.8365         0.1194         0.3258         0.7713         0.0574         0.2422           0.15         1.0143         0.3184         0.5409         0.8237         0.1209         0.3231         0.7013         0.0610         0.2428           0.16         1.0070         0.3174         0.5328         0.7914         0.1212         0.3207         0.6879         0.0624         0.2406           0.17         1.0000         0.3167         0.5328         0.7715         0.1241         0.3161         0.6589         0.0649         0.2365           0.18         0.9933         0.3160         0.5225         0.7756         0.1254         0.3079         0.6421         0.0669         0.2327           0.22         0.9690         0.3125         0.5201         0.7576         0.1263         0.3079         0.6342         0.0683         0.2215           0.23         0.9633         0.3115         0.5152         0.7368         0.1271         0.3025         0.6126         0.0707         0.2228 <td>0.11</td> <td>1.0489</td> <td>0.3187</td> <td>0.5496</td> <td></td> <td>0.8662</td> <td>0.1155</td> <td>0.3315</td> <td>0.7421</td> <td>0.0553</td> <td>0.2504</td>	0.11	1.0489	0.3187	0.5496		0.8662	0.1155	0.3315	0.7421	0.0553	0.2504
0.13         1.0304         0.3187         0.5437         0.8365         0.1194         0.3258         0.7138         0.0593         0.2422           0.14         1.0221         0.3184         0.5409         0.8237         0.1209         0.3231         0.7013         0.0610         0.2428           0.15         1.0143         0.3180         0.5381         0.8121         0.1222         0.3207         0.6689         0.0624         0.2365           0.16         1.0000         0.3167         0.5328         0.7914         0.1232         0.3183         0.6689         0.0649         0.2365           0.18         0.9933         0.3160         0.5320         0.7735         0.1248         0.3119         0.6594         0.0659         0.2327           0.20         0.9869         0.3152         0.5276         0.7576         0.1263         0.3079         0.6421         0.0677         0.2309           0.21         0.9747         0.3134         0.5252         0.7576         0.1263         0.3079         0.6342         0.6194         0.6057         0.2275           0.23         0.9630         0.3152         0.5128         0.7368         0.1270         0.3025         0.6164         0.0697 <td>0.12</td> <td>1.0393</td> <td>0.3188</td> <td>0.5466</td> <td></td> <td>0.8506</td> <td>0.1177</td> <td>0.3285</td> <td>0.7273</td> <td>0.0574</td> <td>0.2477</td>	0.12	1.0393	0.3188	0.5466		0.8506	0.1177	0.3285	0.7273	0.0574	0.2477
0.14         1.021         0.3184         0.5409         0.8237         0.1209         0.3231         0.7013         0.0610         0.2428           0.15         1.0043         0.3180         0.5381         0.8121         0.1222         0.3207         0.66897         0.0624         0.2406           0.16         1.0070         0.3174         0.5328         0.7914         0.1212         0.3183         0.66897         0.0624         0.2406           0.18         0.9933         0.3160         0.5328         0.7914         0.1241         0.3161         0.6594         0.0659         0.2325           0.20         0.9867         0.3143         0.5250         0.7556         0.1254         0.3119         0.6505         0.0649         0.2227           0.9600         0.3125         0.5216         0.7756         0.1263         0.3079         0.6421         0.0677         0.229           0.22         0.9603         0.3115         0.5176         0.7434         0.1266         0.3042         0.6126         0.0601         0.22275           0.224         0.9579         0.3105         0.5152         0.7368         0.1271         0.3025         0.6126         0.0703         0.2243	0.13	1.0304	0.3187	0.5437		0.8365	0.1194	0.3258	0.7138	0.0593	0.2452
0.15         1.0143         0.3180         0.5381         0.8121         0.1222         0.3207         0.66897         0.0624         0.2406           0.16         1.0070         0.3174         0.5354         0.8014         0.1232         0.3183         0.6789         0.0637         0.2385           0.17         1.0000         0.3167         0.5328         0.7914         0.12241         0.3161         0.6689         0.0639         0.2365           0.18         0.9933         0.3160         0.5322         0.7735         0.1254         0.3119         0.6505         0.2365           0.20         0.9807         0.3143         0.5250         0.7576         0.1253         0.3079         0.6421         0.0665         0.2291           0.22         0.9630         0.3155         0.5201         0.7504         0.1266         0.3042         0.6144         0.0697         0.2259           0.23         0.9633         0.3105         0.5172         0.7368         0.1271         0.3025         0.6126         0.0703         0.2243           0.525         0.3095         0.5128         0.7305         0.1271         0.3027         0.22233           0.242         0.3074         0.5081	0.14	1.0221	0.3184	0.5409		0.8237	0.1209	0.3231	0.7013	0.0610	0.2428
0.16         1.0070         0.3174         0.5354         0.8014         0.1232         0.3183         0.6789         0.0637         0.2385           0.17         1.0000         0.3167         0.5328         0.7914         0.1241         0.3161         0.6689         0.0649         0.2365           0.18         0.9933         0.3160         0.5302         0.7822         0.1248         0.3119         0.6505         0.0669         0.2345           0.20         0.9807         0.3134         0.5250         0.7576         0.1263         0.3099         0.6421         0.0677         0.2309           0.21         0.9690         0.3125         0.5201         0.7504         0.1266         0.3061         0.6626         0.0691         0.2275           0.23         0.9633         0.3115         0.5172         0.7305         0.1270         0.3007         0.6061         0.0707         0.2228           0.24         0.9579         0.3105         0.5128         0.7305         0.1271         0.3007         0.6126         0.0703         0.2243           0.24         0.9573         0.3063         0.5081         0.71745         0.1272         0.2991         0.5988         0.0712         0.2213 <td>0.15</td> <td>1.0143</td> <td>0.3180</td> <td>0.5381</td> <td></td> <td>0.8121</td> <td>0.1222</td> <td>0.3207</td> <td>0.6897</td> <td>0.0624</td> <td>0.2406</td>	0.15	1.0143	0.3180	0.5381		0.8121	0.1222	0.3207	0.6897	0.0624	0.2406
0.17         1.0000         0.3167         0.5328         0.7914         0.1241         0.3161         0.6689         0.0649         0.2365           0.18         0.9933         0.3160         0.5302         0.7822         0.1248         0.3139         0.6594         0.0659         0.2345           0.19         0.9860         0.3152         0.5276         0.7735         0.1254         0.3119         0.6690         0.2327           0.20         0.9807         0.3143         0.5250         0.7576         0.1263         0.3079         0.6421         0.0677         0.2309           0.21         0.9747         0.3115         0.5176         0.7576         0.1263         0.3079         0.6142         0.0687         0.2275           0.23         0.9633         0.3115         0.5176         0.7434         0.1268         0.3042         0.6194         0.0697         0.2259           0.24         0.9579         0.3105         0.5128         0.7305         0.1271         0.3025         0.6126         0.0707         0.22283           0.25         0.9473         0.3085         0.5108         0.7130         0.1272         0.2991         0.5998         0.0712         0.2213	0.16	1.0070	0.3174	0.5354		0.8014	0.1232	0.3183	0.6789	0.0637	0.2385
0.18         0.9933         0.3160         0.5302         0.7822         0.1248         0.3139         0.6594         0.0659         0.2345           0.19         0.9869         0.3152         0.5276         0.7735         0.1254         0.3119         0.6594         0.0659         0.2327           0.20         0.9807         0.3143         0.5250         0.7536         0.1263         0.3099         0.6421         0.0677         0.2309           0.21         0.9747         0.3134         0.5225         0.7576         0.1266         0.3061         0.6266         0.0691         0.2275           0.23         0.9633         0.3115         0.5176         0.7434         0.1268         0.3042         0.6194         0.0697         0.2243           0.25         0.9525         0.3095         0.5128         0.7305         0.1271         0.3007         0.6061         0.0707         0.2288           0.27         0.9422         0.3074         0.5081         0.7186         0.1272         0.2914         0.5938         0.0715         0.2185           0.28         0.9373         0.3063         0.5036         0.7076         0.1272         0.2942         0.5825         0.0722         0.2171 <td>0.17</td> <td>1.0000</td> <td>0.3167</td> <td>0.5328</td> <td></td> <td>0.7914</td> <td>0.1241</td> <td>0.3161</td> <td>0.6689</td> <td>0.0649</td> <td>0.2365</td>	0.17	1.0000	0.3167	0.5328		0.7914	0.1241	0.3161	0.6689	0.0649	0.2365
	0.18	0.9933	0.3160	0.5302		0.7822	0.1248	0.3139	0.6594	0.0659	0.2345
	0.19	0.9869	0.3152	0.5276		0.7735	0.1254	0.3119	0.6505	0.0669	0.2327
	0.20	0.9807	0.3143	0.5250		0.7653	0.1259	0.3099	0.6421	0.0677	0.2309
0.22         0.9690         0.3125         0.5201         0.7504         0.1266         0.3042         0.6266         0.0691         0.2275           0.23         0.9633         0.3115         0.5176         0.7434         0.1268         0.3042         0.6194         0.0697         0.2259           0.24         0.9579         0.3105         0.5152         0.7368         0.1270         0.3025         0.6126         0.0703         0.2243           0.25         0.9422         0.3074         0.5081         0.7365         0.1272         0.2991         0.5998         0.0712         0.2218           0.27         0.9422         0.3074         0.5081         0.7136         0.1272         0.2958         0.5881         0.0719         0.2185           0.29         0.9324         0.3053         0.5036         0.7076         0.1272         0.2942         0.5825         0.0722         0.2171           0.30         0.9276         0.3042         0.5013         0.7024         0.1270         0.2911         0.5772         0.0724         0.2185           0.31         0.9297         0.3031         0.4991         0.6878         0.1269         0.2896         0.5670         0.0722         0.2132 <td>0.21</td> <td>0.9747</td> <td>0.3134</td> <td>0.5225</td> <td></td> <td>0.7576</td> <td>0.1263</td> <td>0.3079</td> <td>0.6342</td> <td>0.0685</td> <td>0.2291</td>	0.21	0.9747	0.3134	0.5225		0.7576	0.1263	0.3079	0.6342	0.0685	0.2291
	0.22	0.9690	0.3125	0.5201		0.7504	0.1266	0.3061	0.6266	0.0691	0.2275
	0.23	0.9633	0.3115	0.5176		0.7434	0.1268	0.3042	0.6194	0.0697	0.2259
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.24	0.9579	0.3105	0.5152		0.7368	0.1270	0.3025	0.6126	0.0703	0.2243
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.25	0.9525	0.3095	0.5128		0.7305	0.1271	0.3007	0.6061	0.0707	0.2228
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.26	0.9473	0.3085	0.5105	1	0.7245	0.1272	0.2991	0.5998	0.0712	0.2213
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.27	0.9422	0.3074	0.5081	L	0.7186	0.1273	0.2974	0.5938	0.0715	0.2199
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.28	0.9373	0.3063	0.5058	I I	0.7130	0.1272	0.2958	0.5881	0.0719	0.2185
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.29	0.9324	0.3053	0.5036		0.7076	0.1272	0.2942	0.5825	0.0722	0.2171
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.30	0.9276	0.3042	0.5013		0.7024	0.1271	0.2927	0.5772	0.0724	0.2158
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.31	0.9229	0.3031	0.4991		0.6974	0.1270	0.2911	0.5720	0.0727	0.2145
	0.32	0.9183	0.3020	0.4969		0.6925	0.1269	0.2896	0.5670	0.0729	0.2132
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.33	0.9137	0.3009	0.4947		0.6878	0.1268	0.2882	0.5622	0.0730	0.2120
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.34	0.9092	0.2998	0.4925		0.6831	0.1266	0.2867	0.5575	0.0732	0.2108
0.36         0.3003         0.2976         0.4882         0.6743         0.1262         0.2839         0.5486         0.0734         0.2084           0.37         0.8962         0.2965         0.4861         0.6700         0.1260         0.2825         0.5444         0.0735         0.2072           0.38         0.8920         0.2954         0.4840         0.6659         0.1258         0.812         0.5402         0.0735         0.2061           0.39         0.8878         0.2923         0.4799         0.6659         0.1258         0.2812         0.5402         0.0735         0.2061           0.40         0.8877         0.2921         0.4779         0.6579         0.1250         0.2772         0.5284         0.0736         0.2039           0.41         0.8797         0.2921         0.4779         0.6502         0.1270         0.5284         0.0736         0.2028           0.42         0.8757         0.2910         0.4759         0.6502         0.1247         0.759         0.5247         0.0736         0.2007           0.43         0.8717         0.2889         0.4719         0.6465         0.1241         0.2734         0.5175         0.0736         0.2007	0.35	0.9048	0.2987	0.4904		0.6787	0.1264	0.2853	0.5530	0.0733	0.2096
0.37         0.3922         0.2954         0.4801         0.6700         0.1260         0.2825         0.5444         0.0735         0.2072           0.38         0.8920         0.2954         0.4840         0.6659         0.1258         0.2812         0.5402         0.0735         0.2061           0.39         0.8878         0.29243         0.4820         0.6618         0.1258         0.2798         0.5362         0.0736         0.2050           0.40         0.8837         0.2921         0.4779         0.6579         0.1253         0.2778         0.5323         0.0736         0.2039           0.41         0.8797         0.2921         0.4779         0.6540         0.1250         0.2775         0.5284         0.0736         0.2039           0.42         0.8757         0.2910         0.4759         0.6502         0.1247         0.2759 <b>0.5247</b> 0.0736         0.2007           0.42         0.8777         0.2910         0.4759         0.6428         0.1241         0.2734         0.5175         0.0736         0.2007           0.44         0.8678         0.2889         0.4719         0.6428         0.1241         0.2734         0.5175         0.0736         0.1987<	0.30	0.9005	0.29/6	0.4882		0.6743	0.1262	0.2839	0.5486	0.0734	0.2084
0.39         0.2930         0.2943         0.4840         0.009         0.1238         0.2812         0.3402         0.0735         0.2061           0.39         0.8878         0.2943         0.4820         0.6618         0.1255         0.2798         0.5362         0.0736         0.2050           0.40         0.8837         0.2932         0.4799         0.6579         0.1253         0.2785         0.5362         0.0736         0.2039           0.41         0.8797         0.2921         0.4799         0.6579         0.1250         0.2772         0.5284         0.0736         0.2028           0.42         0.8757         0.2910         0.4759         0.6502         0.1247         0.2759         0.5247         0.0736         0.2028           0.43         0.8717         0.2889         0.4719         0.6465         0.1244         0.2746         0.5211         0.0736         0.2007           0.44         0.8678         0.2889         0.4719         0.6428         0.1244         0.2744         0.5175         0.0736         0.1997           0.45         0.8640         0.2867         0.4680         0.6327         0.1235         0.2719         0.5106         0.0735         0.1977	0.37	0.8902	0.2905	0.4801		0.6700	0.1260	0.2825	0.5444	0.0735	0.2072
0.39         0.3818         0.2932         0.4820         0.6818         0.1255         0.2798         0.3362         0.0736         0.2050           0.40         0.8837         0.2932         0.4799         0.6579         0.1253         0.2778         0.5362         0.0736         0.2039           0.41         0.8797         0.2921         0.4779         0.6540         0.1253         0.2772         0.5284         0.0736         0.2028           0.42         0.8757         0.2910         0.4759         0.6502         0.1247         0.2772         0.5284         0.0736         0.2028           0.43         0.8717         0.2899         0.4739         0.6465         0.1244         0.2746         0.5211         0.0736         0.2007           0.44         0.8678         0.2899         0.4719         0.6465         0.1244         0.2746         0.5115         0.0736         0.2007           0.45         0.8640         0.2878         0.4700         0.6392         0.1238         0.2721         0.5140         0.0736         0.1987           0.46         0.8601         0.2867         0.4680         0.6323         0.1232         0.2709         0.5106         0.0735         0.1977 <td>0.36</td> <td>0.8920</td> <td>0.2954</td> <td>0.4840</td> <td></td> <td>0.6659</td> <td>0.1258</td> <td>0.2812</td> <td>0.5402</td> <td>0.0735</td> <td>0.2061</td>	0.36	0.8920	0.2954	0.4840		0.6659	0.1258	0.2812	0.5402	0.0735	0.2061
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.39	0.0027	0.2943	0.4820		0.0018	0.1255	0.2798	0.5362	0.0736	0.2050
0.41         0.8757         0.2910         0.4779         0.6540         0.1250         0.2772         0.5284         0.0736         0.2028           0.42         0.8757         0.2910         0.4759         0.6502         0.1247         0.2759         0.5247         0.0736         0.2018           0.43         0.8717         0.2899         0.4739         0.6465         0.1244         0.2746         0.5211         0.0736         0.2007           0.44         0.8678         0.2889         0.4719         0.6428         0.1241         0.2746         0.5115         0.0736         0.2007           0.45         0.8640         0.2878         0.4700         0.6428         0.1241         0.2734         0.5175         0.0736         0.1997           0.46         0.8601         0.2867         0.4680         0.6357         0.1235         0.2709         0.5140         0.0736         0.1987           0.47         0.8564         0.2856         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1967           0.48         0.8526         0.2846         0.46621         0.6328         0.1232         0.2697         0.5073         0.0734         0.1957 <td>0.40</td> <td>0.8837</td> <td>0.2932</td> <td>0.4799</td> <td></td> <td>0.6579</td> <td>0.1253</td> <td>0.2785</td> <td>0.5323</td> <td>0.0736</td> <td>0.2039</td>	0.40	0.8837	0.2932	0.4799		0.6579	0.1253	0.2785	0.5323	0.0736	0.2039
0.42         0.8717         0.2819         0.4739         0.6302         0.1247         0.2759         0.5247         0.0736         0.2018           0.43         0.8717         0.2899         0.4739         0.6465         0.1244         0.2746         0.5211         0.0736         0.2007           0.44         0.8678         0.2899         0.4739         0.6465         0.1244         0.2734         0.5175         0.0736         0.2007           0.45         0.8640         0.2878         0.4700         0.6428         0.1241         0.2734         0.5175         0.0736         0.1997           0.46         0.8601         0.2867         0.4680         0.6357         0.1235         0.2709         0.5106         0.0735         0.1987           0.47         0.8564         0.2856         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1987           0.47         0.8556         0.2866         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1967           0.48         0.82526         0.2846         0.4632         0.6389         0.1232         0.2697         0.5073         0.0734         0.1957 <td>0.41</td> <td>0.0757</td> <td>0.2921</td> <td>0.4779</td> <td></td> <td>0.6540</td> <td>0.1250</td> <td>0.2772</td> <td>0.5284</td> <td>0.0736</td> <td>0.2028</td>	0.41	0.0757	0.2921	0.4779		0.6540	0.1250	0.2772	0.5284	0.0736	0.2028
0.44         0.2679         0.4739         0.6465         0.1244         0.2746         0.5211         0.0736         0.2007           0.44         0.8678         0.2889         0.4719         0.6428         0.1241         0.2734         0.5175         0.0736         0.1997           0.45         0.8640         0.2878         0.4700         0.6392         0.1238         0.2721         0.5140         0.0736         0.1987           0.46         0.8601         0.2867         0.4680         0.6327         0.1235         0.2709         0.5106         0.0735         0.1987           0.47         0.8564         0.2856         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1977           0.47         0.8526         0.2846         0.4621         0.6323         0.1232         0.2697         0.5073         0.0735         0.1967           0.48         0.8526         0.2846         0.4632         0.6323         0.1232         0.2697         0.5073         0.0734         0.1957           0.49         0.8489         0.2835         0.6363         0.1232         0.2697         0.5073         0.0734         0.1957 <td>0.42</td> <td>0.0/3/</td> <td>0.2910</td> <td>0.4730</td> <td></td> <td>0.6502</td> <td>0.1247</td> <td>0.2759</td> <td>0.5247</td> <td>0.0736</td> <td>0.2018</td>	0.42	0.0/3/	0.2910	0.4730		0.6502	0.1247	0.2759	0.5247	0.0736	0.2018
0.45         0.8640         0.2878         0.4700         0.6392         0.1241         0.2721         0.5175         0.0736         0.1997           0.46         0.8640         0.2878         0.4700         0.6392         0.1238         0.2721         0.5140         0.0736         0.1987           0.46         0.8601         0.2867         0.4680         0.6392         0.1238         0.2721         0.5166         0.0736         0.1987           0.47         0.8564         0.2856         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1977           0.48         0.8526         0.2856         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1967           0.48         0.8526         0.2846         0.4642         0.6289         0.1232         0.2697         0.5041         0.0734         0.1957           0.49         0.8489         0.1232         0.2697         0.5041         0.0734         0.1957	0.43	0.8/1/	0.2899	0.4739		0.0403	0.1244	0.2746	0.5211	0.0736	0.2007
0.46         0.8601         0.2867         0.4680         0.6332         0.1235         0.2712         0.5140         0.0735         0.1987           0.47         0.8604         0.2867         0.4680         0.6337         0.1235         0.2709         0.5106         0.0735         0.1987           0.47         0.8564         0.2866         0.4661         0.6323         0.1232         0.2697         0.5106         0.0735         0.1987           0.48         0.8526         0.2866         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1967           0.48         0.8526         0.2846         0.46621         0.6329         0.1232         0.2697         0.5073         0.0734         0.1957           0.49         0.8498         0.1239         0.2697         0.5041         0.0734         0.1957	0.44	0.8640	0.2889	0.4700		0.6202	0.1241	0.2734	0.5175	0.0736	0.1997
0.40         0.207         0.400         0.637         0.1235         0.2/09         0.3106         0.0735         0.1977           0.47         0.8564         0.2886         0.4661         0.6323         0.1232         0.2697         0.5073         0.0735         0.1977           0.48         0.8526         0.2846         0.4642         0.6289         0.1229         0.2687         0.5041         0.0734         0.1957           0.49         0.8489         0.2835         0.64631         0.6326         0.1229         0.2687         0.5001         0.0734         0.1957	0.45	0.8040	0.2070	0.4700		0.6392	0.1236	0.2721	0.5140	0.0736	0.1987
0.48 0.8526 0.2846 0.4642 0.6289 0.1232 0.2697 0.5041 0.0735 0.1967 0.48 0.8526 0.2846 0.4642 0.6289 0.1229 0.2685 0.5041 0.0734 0.1957 0.49 0.8489 0.2835 0.50453 0.6269 0.1276 0.2675	0.40	0.8564	0.2007	0.4080		0.0337	0.1233	0.2/09	0.5106	0.0735	0.1977
0.49 0.5020 0.4042 0.0289 0.1229 0.2085 0.5041 0.0754 0.1957 0.49 0.9585 0.5000 0.0754 0.1957	0.48	0.8526	0.2000	0.4642		0.0323	0.1232	0.2097	0.5073	0.0735	0.1967
	0.40	0.8489	0 2835	0.4621		0.6256	0.1229	0.2083	0.5041	0.0734	0.1957

Note: Overall Credibility (D x Zp) + ((1 - D) x Ze), where D is the empirical D-ratio for the group. Valid combinations of Zp and Ze are those for which Zp and Ze are bounded by [0,1].

Exhibit 1

## CALIFORNIA EXPERIENCE RATING PLAN

RIDGE REGRESSION RESULTS Projection Year 1991 5th Report



Exhibit 2

## CALIFORNIA EXPERIENCE RATING PLAN

347

MAXIMUM EXCESS RIDGE REGRESSION CREDIBILITIES Projection Year 1991 at 5th Report - Iteration 0

		Median	1997 Ex	perience	Exp Period		Maxim	um Excess			
		Exper. Period	Ratin	g Plan	Empirical	Ridge Regression Values*			s*	Fitted	Values
Ris	ks	Expected Loss	Zp	Ze	D Ratio	θ	Zp	Ze	Overall	Zp	Ze
1 -	5k	520,196	0.98381	0.37463	0.31619	0.17	0.99999	0.31674	0.53277	0.95084	0.32174
5k -	10k	209,397	0.95602	0.23796	0.29807	0.22	0.90989	0.21842	0.42453	0.88214	0.21834
10k -	15k	130,614	0.92729	0.17917	0.29403	0.16	0.87377	0.19318	0.39329	0.82059	0.17218
15k -	20k	94,331	0.89826	0.14421	0.29252	0.25	0.73658	0.14503	0.31807	0.76510	0.14369
20k -	25k	73,038	0.86864	0.11991	0.28773	0,27	0.71864	0.12725	0.29741	0.71380	0.12322
25k -	30k	58,775	0.83801	0.10137	0.29156	0.58	0.62907	0.09186	0.24849	0.66535	0.10714
30k -	35k	48,710	0.80709	0.08684	0.28371	0.30	0.61032	0,09719	0.24277	0.62040	0.09419
35k -	40k	41,539	0.77752	0.07555	0.28733	0.78	0.47275	0.05385	0.17421	0.58056	0.08388
40k -	45k	35,917	0.74781	0.06602	0.28722	0.52	0.58135	0.07679	0.22171	0.54323	0.07498
45k -	50k	31,528	0.71903	0.05807	0.28404	0.42	0.52471	0.07364	0.20177	0.50934	0.06742
50k -	55k	27,940	0.69065	0.05120	0.28807	0,65	0.55995	0.06828	0.20992	0.47785	0.06074
55k -	60k	24,984	0.66303	0.04523	0.28579	0.56	0.42228	0.05234	0.15806	0.44884	0.05485
60k -	65k	22,444	0.63545	0.03984	0.28890	0.82	0.36133	0.03880	0.13198	0.42136	0.04943
65k -	70k	20,297	0.60875	0.03508	0.28551	0.61	0,36762	0.04313	0.13577	0.39601	0.04457
70k -	75k	18,366	0.58154	0.03061	0.28546	0.42	0.40716	0.05187	0.15329	0.37135	0.03993
75k -	80k	16,696	0.55512	0.02657	0.28212	0.69	0.40919	0.04364	0.14677	0.34845	0.03568
80k -	85k	15,175	0.52833	0.02275	0.28821	0,33	0.43899	0.06078	0.16978	0.32617	0.03160
85k -	90k	13,641	0.49826	0.01874	0.28056	0,38	0.43581	0.05543	0.16215	0.30222	0.02723
90k -	95k	12,083	0.46406	0.01447	0.27956	0.75	0,25916	0.02758	0.09232	0.27622	0.02250
95k -	100k	10,278	0.41901	0.00923	0.26503	1.03	0.20355	0.01676	0.06626	0.24378	0.01656

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\*Values along the ridge trace where excess credibility is maximized, with primary and excess credibilities bounded by [0,1].

\*\*Data not used in credibility smoothing. Adjusted R<sup>2</sup> of fits: 0.93, Zp; 0.97, Ze.



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Exhibit 4 Part 1



Zp ~ Logistic (10.32, 0.96)

## CALIFORNIA EXPERIENCE RATING PLAN DEVELOPMENT OF RATING VALUES / 1991 5th Report - Iteration 0 Excess Credibility / Ze = [1/(1 + exp[(14.1151 - X) / 1.92436)] - 0.0569084





349

CALIFORNIA EXPERIENCE RATING PLAN

Exhibit 5

DERIVATION OF B AND W VALUES FROM PRIMARY AND EXCESS CREDIBILITIES Projection Year: 1991 5th Report - Iteration 0



# CALIFORNIA EXPERIENCE RATING PLAN TABLE OF B AND W VALUES Projection Year: 1991 at 5th Report - Iteration 0

					_		
Expect	ed			Expec	ted		
Losse	5	w	В	1.055	25	**	B
9 750	0.010	0.06	22 124	1.015.097	2 077 263	0.50	25 272
0,750 -	9,019	0.05	32,124	1,713,967 -	2,077,303	0.50	25,575
9,020 -	11 142	0.00	21 947	2,077,304 -	2,232,032	0.51	15 105
3,353 -	12 677	0.07	31,647	2,232,033 -	2,445,802	0.52	25,105
11,144 -	12,077	0.08	31,080	2,445,805 -	2,032,114	0.33	25,100
12,078 -	14,720	0.09	51,489	2,052,115 -	2,879,404	0.54	25,017
14,721 -	17,508	0.10	31,268	2,879,465 -	3,128,044	0.55	24,927
17,509 -	21,361	0.11	31,015	3,128,045 -	3,400,278	0.56	24,838
21,362 -	26,619	0.12	30,733	3,400,279 -	3,698,937	0.57	24,748
26,620 -	33,502	0.13	30,434	3,698,938 -	4,027,195	0.58	24,657
33,503 -	42,022	0.14	30,134	4,027,196 -	4,388,699	0.59	24,566
42,023 -	52,053	0.15	29,849	4,388,700 -	4,787,661	0.60	24,474
52,054 -	63,464	0.16	29,584	4,787,662 -	5,228,959	0.61	24,381
63,465 -	76,178	0.17	29,342	5,228,960 -	5,718,269	0.62	24,287
76,179 -	90,172	0.18	29,120	5,718,270 -	6,262,224	0.63	24,193
90,173 -	105,460	0.19	28,916	6,262,225 -	6,868,610	0.64	24,097
105,461 -	122,087	0.20	28,728	6.868.611 -	7,546,617	0.65	23,999
122.088 -	140.115	0.21	28,552	7.546.618 -	8.307.147	0.66	23,901
140 116 -	159,619	0.22	28 387	8 307 148 -	9 163 208	0.67	23 800
159 620 -	180,688	0.23	28,231	9 163 209 -	10 130 416	0.68	23,698
180,689	203 420	0.24	28.083	10 130 417 -	11 227 642	0.60	23 594
100,002	203,420	0.24	20,005	10,150,417 -	11,227,042	0.07	23,374
203,421 -	227,925	0.25	27,942	11,227,643 -	12,477,859	0.70	23,487
227,926 -	254,321	0.26	27,807	12,477,860 -	13,909,243	0.71	23,378
254,322 -	282,740	0.27	27,678	13,909,244	15,556,644	0.72	23,267
282,741 -	313,323	0.28	27,553	15,556,645 -	17,463,567	0.73	23,152
313,324 -	346,226	0.29	27,433	17,463,568 -	19,684,858	0.74	23,034
346,227 -	381,615	0.30	27,316	19.684.859 -	22,290,427	0.75	22,913
381,616 -	419,674	0.31	27,202	22,290,428 -	25,370,463	0.76	22,787
419,675 -	460,603	0.32	27,091	25,370,464 -	29,042,880	0.77	22,656
460,604 -	504,618	0.33	26,983	29,042,881 -	33,464,157	0.78	22,521
504,619 -	551,956	0.34	26,878	33,464,158 -	38,845,437	0.79	22,379
551,957 -	602,876	0.35	26,774	38,845,438 -	45,477,054	0.80	22,230
602,877 -	657,660	0.36	26,673	45,477,055 -	53,766,874	0.81	22,074
657,661 -	716,618	0.37	26,573	53,766,875 -	64,302,165	0.82	21,908
716,619 -	780,090	0.38	26,475	64,302,166 -	77,953,021	0.83	21,732
780,091 -	848,447	0.39	26,378	77,953,022 -	96,052,589	0.84	21,543
848.448 -	922.099	0.40	26.283	96,052,590 -	120,726.940	0.85	21,339
922.100 -	1.001.497	0.41	26,189	120.726.941 -	155,535,462	0.86	21.116
1.001.498 -	1.087.138	0.42	26.096	155.535.463 -	206,807,256	0.87	20.869
1 087 139 -	1 179 571	0.43	26 003	206 807 257 -	286 695 068	0.88	20 591
1.179.572 -	1,279,404	0.44	25,912	286,695,069 -	421.029.234	0.89	20,272
1 279 405	1 797 217	0.44	25 921	421 020 225	673 045 313	0.90	10 903
1,2/9,403 -	1,387,312	0.42	23,821	421,029,233 -	073,043,311	0.90	19,893
1,387,313 -	1,504,041	0.40	43,730	073,045,312 -	1,234,122,861	0.91	19,419
1,204,042 -	1,030,420	0.4/	25,040	1,234,122,802 -	2,930,427,391	0.92	18,772
1,030,427 -	1,101,395	0.48	23,331				
1,/0/,390 -	1,915,986	0.49	20,402				
				l			

Exhibit 6

#### CALIFORNIA EXPERIENCE RATING PLAN QUINTILES TESTS Projection Year: 1991 5th Report

#### Iteration 0

Standard Loss	Ratio					
Indicated Modification		Exp	ected Loss Qui	ntiles		}
Quintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.572	0.491	0.487	0.491	0.542	0.571
Low	0.625	0.550	0.528	0.491	0.633	0.603
Middle	0.629	0.589	0.567	0.593	0.633	0.621
High	0.638	0.641	0.618	0.630	0.628	0.642
Highest	0.622	0.639	0.657	0.633	0.743	0.627
All Risks	0.620	0.592	0.582	0.575	0.640	0.613

Indicated Modification		Expe	cted Loss Qui	ntiles		
Ouintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.394	0.373	0.401	0.427	0.486	0.426
Low	0.513	0.457	0.446	0.427	0.596	0.515
Middle	0.577	0.538	0.511	0.540	0.596	0.588
High	0.677	0.671	0.632	0.634	0.629	0.663
Highest	0.865	0.879	0.873	0.820	0.935	0.840
All Risks	0.598	0.583	0.574	0.571	0.644	0.595

352

Standard Loss	Ratio					
Indicated Mod		Expec	ted Loss Quir	tile		
Ouintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.587	0.524	0.489	0.534	0.561	0.575
Low	0.632	0.550	0.547	0.534	0.587	0.621
Middle	0,634	0.597	0.599	0.589	0.687	0.628
High	0,635	0.626	0 609	0.629	0.636	0.635
Highest	0.614	0.628	0.631	0.602	0.701	0.618
All Risks	0.622	0.594	0.585	0.577	0.639	0.615

Iteration	1
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Indicated Mod		Expec	ted Loss Quir	ntile		
Ouintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.394	0.382	0.376	0.452	0.490	0.411
Low	0.513	0.439	0.444	0.452	0.520	0.530
Middle	0.578	0.541	0.533	0.516	0.648	0.577
High	0.677	0.661	0.633	0.645	0.646	0.663
Highest	0.866	0.892	0.877	0.828	0.938	0.851
All Risks	0.598	0.583	0.574	0.571	0.644	0.595

Indicated Modification		Ехра	ected Loss Qui	ntiles		
Quintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.595	0.531	0.514	0.500	0.575	0.579
Low	0.632	0.558	0.544	0.568	0.592	0.623
Middle	0.635	0.599	0.611	0.601	0.667	0.629
High	0.635	0.626	0.601	0.618	0.633	0.633
Highest	0.613	0.620	0.621	0.583	0.710	0.615
All Risks	0.622	0.595	0.586	0.578	0.640	0.616

Indicated Modification		Expe	cted Loss Qui	ntiles		1
Ouintile	Largest	Large	Middle	Small	Smallest	All Risks
Lowest	0.395	0.375	0.383	0.389	0.493	0.403
Low	0.513	0.440	0.420	0.473	0.522	0.520
Middle	0.579	0.541	0.544	0.523	0.636	0.576
High	0.676	0.663	0.629	0.642	0.648	0.664
Highest	0.866	0.893	0.886	0.825	0.940	0.854
All Risks	0.598	0.583	0.574	0.571	0.644	0.595

#### CALIFORNIA EXPERIENCE RATING PLAN

ITERATIVE PARAMETER REFINEMENT Projection Year: 1991 5th Report - Iteration 0

					Expec	cted Loss Quir	ntiles					
	Quint	ile#1	Quint	ile #2	Quint	ile #3	Quint	ile #4	Quint	ile #5	ĂII F	lisks
Projected	Number	Std Loss	Number	Std Loss	Number	Std Loss	Number	Std Loss	Number	Std Loss	Number	Std Loss
Mod	of Risks	Ratio	of Risks	Ratio	of Risks	Ratio	of Risks	Ratio	of Risks	Ratio	of Risks	Ratio
0.0												
0.1												
0.2												
0.3												
0.4	2	1.013									2	1.013
0.5	11	0.339									11	0.339
0,6	167	0.496									167	0.496
0.7	1,703	0.573	165	0.385							1,868	0.569
0.8	3,666	0.583	4,840	0.497	1,453	0.423					9,959	0.561
0.9	3,782	0.643	4,567	0.566	8,470	0.528	9,835	0.491	4,507	0.530	31,161	0.603
1.0	3,249	0.623	3,366	0.602	3,433	0.597	3,894	0.672	13,247	0.633	27,189	0.622
1.1	2,485	0.658	2,335	0.655	2,507	0.627	2,460	0.602	3,010	0.624	12,797	0.652
1.2	1,646	0.594	1,681	0.642	1,568	0.640	1,556	0.625	2,232	0.724	8,683	0.610
1.3	1,086	0.594	1,078	0.657	936	0.671	904	0.651	1,104	0.749	5,108	0.613
1.4	763	0.615	700	0.600	611	0.616	535	0.601	628	0.713	3,237	0.615
1.5	512	0.658	462	0.640	368	0.649	323	0.644	330	0.827	1,995	0.658
1.6	296	0.608	269	0.618	239	0.632	189	0.528	185	0.932	1,178	0.616
1.7	212	0.757	167	0.617	141	0.740	125	0.547	111	0.925	756	0.731
1.8	134	0.689	130	0.708	93	0.649	63	0.931	51	0.678	471	0.695
1.9	75	0.603	82	0.620	48	0.878	40	0.904	41	0.603	286	0.631
2.0	61	0.548	44	0.682	34	0.752	24	0.569	22	0.839	185	0.575
2.1	41	0.625	29	0.596	32	0.790	19	0.441	9	0.833	130	0.630
2.2	23	0.703	24	0.698	21	0.892	11	1.318	8	0.262	87	0.717
2.3	18	0.694	14	0.383	16	0.530	6	1.118	7	1.174	61	0.657
2.4	13	0.487	16	0.760	9	0.203	3	2.489	4	0.663	45	0.516
2.5	15	0.657	10	0.896	6	1.807	5	0.220			36	0.695
2.6	6	0.725	5	0.888			1	0.154	1	0.000	13	0.714
2.7	4	0.977	4	0.139	4	0.789					12	0.657
2.8	3	1.146	2	0.856	2	0.699	1	0.635	3	2.743	11	1.188
2.9	7	0.629	2	0.425	1	0.050			2	0.432	12	0.589
3.0	2	0.841			1	0.000					3	0.832
>3.0	18,	0.562	8	1.306	7	0.995	6	1.287	1	0.000	40	0.644
Total	20,000	0.620	20,000	0.592	20,000	0.582	20,000	0.575	25,503	0.640	105,503	0.613

Notes:

353

1. The Indicated Modification shown is the upper bound for the row. Therefore, the expected Indicated Mod for the 1.0 row is 0.95.

#### CALIFORNIA EXPERIENCE RATING PLAN ITERATIVE PARAMETER REFINEMENT Risk-Weighted Regression Output Projection Year: 1991 5th Report - Iteration 0

#### Quintile ]

354

Weighted Regi	cession /	Analysi	5				
Dependent var	iable: S	ud_LR					
Parameter		Estim	ate	Standard Error	7 Statis	tic I	P-Value
CONSTANT	0.05	0.568	885 85909	0.025802 0.02538	2 198	2.048 1.9138	0.0000 8 0.0687
	Analy	nis of V	Verien	ce.			
Source	Sum of	Square	s I	of Mean Se	lute	F-Ratio	P-Value
Model Residual	3.6 22	8357 .1258	1 22	3.68357 1.00572	3.66	0.00	587
Total (Corr.)	2	5.8093	23				
R-squared = 14 R-squared (adj Standard Error Moan absolute Durbin-Watson	. 2722 p insted fo of Est. error = a statisti	ercent c d f.) = 1.002 0.0283 ic = 1.7	= 10.3 285 1059 10045	755 percent	t		

Parameter	E	stimate	Standard Error	T Statistic	p.\	/slue
CONSTANT PROI_MOD	0.05	395065 0.190755	0 039438- 0.03906	1 10.0 22 4.8	173 8336	0.0000 0.0001
	Analysia Sum of Sc	of Varian	yce Y Menn Sr			P.Value
Model	44.76	96 1	44.7696	23.85	0.000	
Revidual	35.66	97 19	1.87735			

	able: Std_LR		
Parameter	Estim	ste –	Standard T Error Statistic P-Value
CONSTANT PROI_MOD -	0.3125 0.05 0.26	573 2768	0.0496612 6.29412 0.0000 0.0493486 5.32473 0.000
	Analysis of V	/arian	
Source	Sum of Square	3 E	Of Mean Square F-Ratio P-Value
Model Residual	65.3039 39.1555	1 17	65.3039 28.35 0.0001 2.30326
	104 450	1.	

Dependent variable: Std_LR											
Parameter		Estim	ate	Standard Error	T Statisti	: P-1	/aluc				
CONSTANT	- <b>0</b> .05	0.320	195 1596	0.0909611 0.09104	1 3.5 02 2	2013 76357	0.0031 0.0145				
	Anal	ysis of \	/arian	æ							
Source	Sum o	( Square	• D	of Mean Sq	puere F	Ratio	P-Value				
Model Residual	47 9	.9631 4.2013	1 15	47.9631 6.28009	7.64	0.0145	i				
Total (Corr.)	1	42.164	16								
R-equared = 3 R-equared (ad Standard Erro	3.7378 junted for r of Est.	percent or d.f.) = = 2.506	- 29.3 01	203 percen	L						

Quintile 5 Weighted Regressio	a Analysis				1	All Rusks Weighted Regressio	m Analysis	-
Dependent variable:	Sud_LR				}	Dependent variable	SId_LR	-
Parameter	Estimate	Standard Error St	T Latistic	P-1	Value	Parameter	Estimate	
CONSTANT PROJ_MOD - 0.05	0.250208 0.383455	0.0694848 0.0684319	3.600 5.60	189 0346	0.0032 0.0001	CONSTANT PROJ_MOD - 0.05	0 540786 0 073540	)
An	alysis of Varian	ce.				An	alysis of Vari	
Source Sum	of Squares D	f Mean Squar	re F-R	atio	P-Value	Source Sum	of Squares	
Model 9 Residual	90.7514 1 37.5737 13	90.7514 3 2.89029	1.40	0.000	1	Model Residual	28.3259 1 53.9003 24	•
Total (Corr.)	128.325 14					Total (Corr.)	82.2262 2	1
R-squared = 70.719 R-squared (adjusted Standard Error of Es Mean absolute error Durbin-Watson stati	<pre>percent for d.f.) = 68.4 at. = 1.70008 = 0.0288783 stic = 2.03497</pre>	676 percent				R-squared = 34.448 R-squared (adjusted Standard Error of E Mean absolute error Durbin-Watson stat	8 percent 1 for d.f.) = 31 st. = 1.49861 r = 0.0158363 intic = 1.6168	I.

Weighted Reg	reasion Analysis					
Dependent va	nable Sid_LR					
Parameter	Estime	de .	Standard Error	T Statist	ic P-1	Value
CONSTANT	0.5407	86	0.0209312	2 25	8363	0.0000
PROJ_MOD	0.05 0.073	5404	0.02070	773	3.55142	0.0016
50urce	20 2250		A Mean ag	10.61	0.001	P-Value
Model Residual	28.3259	1	28.3259	12.61	0.001	6
Total (Corr.)	82.2262	25				
R-squared = 3 R-squared (ad Standard Error	4.4488 percent justed for d.f.) = r of Est. = 1.4984	31.7 61	175 percen	t		

Exhibit 10

## CALIFORNIA EXPERIENCE RATING PLAN ITERATIVE PARAMETER REFINEMENT Projection Year: 1991 5th Report - Iteration 0

Expected Loss Ouintile	Median Risk Rank	Bias Coefficient
Quintile # 1	10,000	0.048591
Quintile # 2	30,000	0.190755
Quintile # 3	50,000	0.262768
Quintile # 4	70,000	0.251596
Quintile # 5	92,752	0,383455
All Risks		0.073540

Regression C	Dutput:
Constant	0.047528
Std Err of Y Est	0.044633
R Squared	0.899567
No. of Observations	5
Degrees of Freedom	3
X Coefficient(s)	3.55892E-06
Std Err of Coef.	6.86560E-07

CALIFORNIA EXPERIENCE RATING PLAN ITERATIVE PARAMETER REFINEMENT Projection Year: 1991 5th Report Exhibit 11



## Plot of Bias Coefficients

## CALIFORNIA EXPERIENCE RATING PLAN ADJUSTMENT OF MAXIMUM EXCESS CREDIBILITIES Projection Year 1991 at 5th Report - Iteration 1

	Iteration 0 Cred.		n 0 Cred.	D Ratio	Overall	Indicated*	Overall		Cred	ibilities			
		Before A	djustment	Based on	Crediblity	Credibility	Credibility		After Adj	ustment***	ŧ.	Fitted	Values
Risk	s	Zp	Ze	Actual Losses	Before Adj.	Adjustments	After Adj.**	Θ	Zp	Ze	Overall	Zp	Ze
1 -	5k	0.95084	0.32174	0.31619	0.52065	0.05643	0.55003	0.17	0.99999	0.31674	0.53277	0.99180	0.32759
5k -	10k	0.88214	0.21834	0.29807	0.41620	0.07422	0.44709	0.13	0.99840	0.21305	0.44714	0.97129	0.20602
10k -	15k	0.82059	0.17218	0.29403	0.36284	0.09201	0.39622	0.15	0.88164	0.19310	0.39555	0.94588	0.15591
15k -	20k	0.76510	0.14369	0.29252	0.32546	0.10981	0.36120	0.08	0.92664	0.12449	0.35914	0.91725	0.12664
20k -	25k	0.71380	0.12322	0.28773	0.29314	0.12760	0.33055	0.11	0.86620	0.11554	0.33152	0.88570	0.10650
25k -	30k	0.66535	0.10714	0.29156	0.26989	0.14540	0.30914	0.22	0.88408	0.07091	0.30800	0.85113	0.09125
30k -	35k	0.62040	0.09419	0.28371	0.24348	0.16319	0.28322	0.09	0.78779	0.08215	0.28235	0.81467	0.07935
35k -	40k	0.58056	0.08388	0.28733	0.22659	0.18099	0.26760	0.14	0.93206	0.00205	0.26928	0.77864	0.07013
40k -	45k	0.54323	0.07498	0.28722	0.20947	0.19878	0.25111	0.30	0.69411	0.07244	0.25100	0.74160	0.06237
45k -	50k	0.50934	0.06742	0,28404	0.19294	0.21658	0.23473	0.18	0.65941	0.06595	0.23451	0.70514	0.05592
50k -	55k	0.47785	0.06074	0.28807	0.18090	0.23437	0.22330	0.52	0.60997	0.06752	0.22378	0.66882	0.05034
55k -	60k	0.44884	0.05485	0.28579	0.16745	0.25217	0.20967	0.14	0.65065	0.03292	0.20946	0.63329	0.04550
60k -	65k	0.42136	0.04943	0.28890	0.15688	0.26996	0.19923	0.17	0.66953	0.00908	0.19988	0.59780	0.04115
65k -	70k	0.39601	0.04457	0.28551	0.14491	0.28776	0.18661	0.14	0.59118	0.02374	0.18575	0.56356	0.03729
70k -	75k	0.37135	0.03993	0.28546	0.13454	0.30555	0.17565	0.20	0.49474	0.04821	0.17568	0.52890	0.03368
75k -	80k	0.34845	0.03568	0.28212	0.12392	0.32334	0.16399	0.47	0.47507	0.04205	0.16422	0.49558	0.03042
80k -	85k	0.32617	0.03160	0.28821	0,11650	0.34114	0.15624	0.49	0.39471	0.05975	0,15629	0.46223	0.02734
85k -	90k	0.30222	0.02723	0.28056	0.10438	0.35893	0.14185	0.65	0.36987	0.05334	0.14215	0.42544	0.02409
90k -	95k	0.27622	0.02250	0.27956	0.09343	0.37673	0.12863	0.20	0.42198	0.01504	0.12881	0.38456	0.02064
<u>95k -</u>	100k	0.24378	0.01656	0.26503	0.07678	0.39452	0,10707	0.20	0.40402	0.00043	0.10739	0.33256	0.01641

\* Credibility Adjustment = 0.047528 + (Rank of median risk) x (3.55892E-06). See Exhibit 10.

\*\* Overall Credibility After Adjustment = Overall Credibility Before Adjustment x [1 + Indicated Credibility Adjustment].

\*\*\* Credibilities along the ridge trace with overall credibility closest to the "Overall Credibility After Adjustment" and with Primary and Excess Credibility values bounded by [0,1].

## CALIFORNIA EXPERIENCE RATING PLAN SUMMARY OF PLAN EFFICIENCIES BY EXPECTED LOSS QUINTILES

Projection Year: 1991 5th Report

			Expected Loss Quintiles							
Manual Premium Weig	hted	Largest 20%	2nd Largest 20%	Middle 20%	2nd Smallest 20%	Smallest 20%	All Risks			
Parameterized B & W	NA	NA	NA	NA	NA	NA				
Frequency Only -1989	NA	NA.	NA	NA	NA	NA				
Promulgated Rating Va	Promulgated Rating Values (based on 1989 3rd)		0.042998	0.029201	0.020843	0.013164	0.068523			
Parameterized	Starting Values	0.129106	0.039685	0.024801	0.017089	0.010145	0.066184			
B & W Plan	Iteration 1	0.129792	0.042418	0.028301	0.019253	0.012138	0.068038			
(based on 1991 5th)	Iteration 2	0.130107	0.043756	0.029928	0.019647	0.011545	0.068829			
· · · · ·	Iteration 3	0.129575	0.044131	0.030589	0.020583	0.010485	0.068709			

358

			Ex	pected Loss Qu	intiles		
Risk Weighted		Largest 20%	2nd Largest 20%	Middle 20%	2nd Smallest 20%	Smallest 20%	All Risks
Parameterized B & W	0.074752	0.024968	0.010343	0.010181	0.007118	0.020767	
Frequency Only -1989	0.081791	0.028444	0.015099	0.013181	0.008131	0.024437	
Promulgated Rating Va	dues (based on 1989 3rd)	0.067791	0.033602	0.025104	0.017707	0.009833	0.024833
Parameterized	Starting Values	0.067418	0.031215	0.021153	0.014610	0.007803	0.023358
B & W Plan	Iteration 1	0.068274	0.033614	0.024102	0.015783	0.009420	0.024758
(based on 1991 5th)	Iteration 2	0,069529	0.034387	0.025760	0.017029	0.009400	0.025815
	Iteration 3	0.069166	0.034830	0.026186	0.017744	0.008103	0.025577

NOTES:

Efficiency is measured as the proportionate reduction in total variance using the following formula:

Efficiency = 
$$E[(u - M)^2 - (u - F)^2]$$
  
 $E[(u - M)^2]$ 

Where E[x] is the expected value function over all risks, u is the Empirical Modification (actual loss / expected loss), M is the Average Empirical Modification for all risks, and F is the Modification under the Plan. This measure of efficiency is discussed by Glenn Meyers in "An Analysis of Experience Rating," PCAS LXXII, 1985, p287. Larger values of efficiency indicate better reproduction of empirical experience.

indicated	1								-					-	Currer	u Modij	fication											_					
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	12	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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0.2	I		<u> </u>																														
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0.4	L	_			1									_																			1
0.5						27	1																										28
0.6				·		6	300	5					-																				311
0.7	<u> </u>		L				127	3,956	1,016																								5.099
0.8						L		461	15,627	3,258															_	-		-			<u> </u>		10 346
0.9	L								525	24,001	862				_																		25 388
1.0			-							4,399	13,836	673																					18 908
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1.3	Τ				1			r				1	813	3,900	584	43	1 · · ·	7	31	21	27	6	1		1		-		-		<u> </u>		5.441
1.4													33	649	2,295	470	59	11			2	5	13	6								<u>+</u>	3 547
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2.3	r							1					<u>t</u>									15	47	32	16		4		· ·			<u> </u>	137
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>10		<u> </u>				<u>+</u> -	<u> </u>						·			t	··· ·					<u>+ · · · </u>		<u> </u>			<u>1</u>		4	3		<u>6</u>	16
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		_	_		1 6		40	1.11.66		1 11 030	12.047	10.939	10.292	2,048	2.701	12.313	11.004	1.146	123	1 511	114	1 211	106	110	- 98	70	- 54		28	21	6	84	1. 105.503

359

Indicated															Cu	rrent M	odificat	ion															
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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0.6						6	299	3				[					_			l					L				I				306
0.7						1	127	2,029	3			I			L.,					1									L		L		2159
0.8								412	2,997	18											1		L		L				L		L	$\vdash$	3.427
0.9						<u> </u>	<u> </u>		350	3,158	54												L		L	L			<b> </b>			<u> </u>	3,562
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21						i						L			I					L	2	26	18	<u> </u>					I		L		46
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2.8																						1							2	2	1		5
2.9																															1	1	2
3.0																														L	1	4	
>3.0																															L	21	21
Total				1	2	33	427	2.444	3.350	3.399	2,905	2.295	1.613	1.081	741	581	329	246	174	100	71	57	37	24	17	13	11	10	. 8	2	3	26	20.000

360

Indicated		_													Cu	rent Me	odificat	ion									-						
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	20	21	2.Z	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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0.8		<u> </u>				1		49	4,139	108														1								L	4,296
0.9								F	124	3,169	94											[										1	3,387
1.0			- · ·	r –						157	2,534	150																	l			L	2,841
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1.4			1				1	I	1					96	574	93	1															l	764
1.5							ł	[	1						69	355	56					L				1		I		-	1		480
1.6				Ι		[	1									58	252	52						L		1					L	-	362
1.7		1					[			Γ							45	156	32					L						· · · · · ·	L		233
1.8		1				1												33	- 96	26													155
1.9		1				1	1												23	74	25							L					122
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2.8						r –		1															l				<u> </u>	2	1	2			5
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Total	1		1	T			1	1.876	4.737	3.434	2.806	2.075	1.573	1.103	744	507	.354	.241	151	120	85	43	40	25	21	13	13	10	6	8	i 1	13	20.000

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Indicated														-	Cu.	ment M	odificer	ion														_	
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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1.5							1								188	307	6				1		1	<del> </del>									501
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1.7							1	<del> </del>								101	132	100	~ 2			t	1	1	t					-		+	330
1.8								-	<u> </u>									119	S.			· · · ·	1	<u> </u>	<u> </u>								172
1.9							-	1											57	34	2		<u>†</u>	1							-		80
2.0								1								-		-	5	54	18	-	<del> </del>	+	-								77
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362

Indicated															Cu	rrent M	odificat	ion															1
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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0.6																								1									
0.7																																	
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0.9										6.075	416													T .									6.491
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1.3												1	331	641	8														<u> </u>				961
1.4	ł												25	251	392									1									668
1.5														6	231	206	3					1	<u> </u>										446
1.6	<u> </u>														18	164	126	1						1									309
1.7															1	26	110	61															198
1.8																1	21	93	39			<u> </u>	1										154
1.9				- · · ·				1										13	53	18		<u> </u>					1				T		84
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22						[													1		9	12	5										27
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2.4																					1	2	3	5	3								14
2.5																							1	3	2	1							7
2.6				1			r					_											1		3	4	1						9
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>3.0	1 · · ·							<u>                                      </u>		· · ·												h	<u> </u>	t			†*		-	4	1	1 7	12
Total	i			i —	<u> </u>	1	· · · ·		2.775	7.870	2.420	2.460	1.732	931	650	397	260	171	115	68	50	29	18	12	12	9	6	2	1	4	t î	7	20.000

363

Indicated															C S	rent Ma	dificati	on															
Mod	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	21	2.2	23	2.4	2.5	2.6	2.7	2.8	2.9	3.0	>3.0	Total
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0.5											1								1	1	1	1											
0.6			1						1				1						1	1	1							1	1	1			
0.7											1			T							1				1								
0.8									167	232	r								1		1				1	1	1	1	1	1			39
0.9									51	8,594	93	1							1		1	· ····		-	1			1		1		-	8,731
1.0			1				[			4.012	4,066	168		1					1		1		-			1							8.24
1.1												1.660	611	188	137	2			1				1		1	1			+				2 596
1.2			[			1		ľ –				9	1.363	606	120	140	76	30	4	1	1				†	1		1	t	ţ	1		2 34
13									-			1	121	686	337	42		7	31	27	27	6	- ī		1	1					t	<u> </u>	1.286
1.4									ſ				8	64	257	234	58	11			2	5	13	6	4	1					1		663
1.5									1		1			2	43	148	180	51	16						5	5	1	3			1		450
1.6									1						2	45	72	97	23	18	3		<u> </u>					1 1	<u> </u>	2	1	3	26
1.7													1			2	29	43	57	13	7	5				T			1		1	2	158
1.8											1						6	26	24	37	16	5	2	3	<u> </u>	1		<u> </u>	t			4	120
1.9																		1	12	20	19	12		4	4	t		t	1		t	T I	27
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364

## CALIFORNIA EXPERIENCE RATING PLAN COMPARISON OF CREDIBLITIES

1997 Plan vs Projection Year 1991

	Median		1997 Experien	ce Rating Plan		1991 Iterati	on 2 (Final)
	Exper. Period	Indicated	i Values	Promulgat	ed Values	Indicated	d Values
Risks	Expected Loss	Zp	Ze	Zp	Ze	Zp	Ze
1 - 5k	520,196	0.98381	0.37463	0.98381	0.36401	0.99949	0.33379
5k - 10k	209,397	0.95602	0.23796	0.95608	0.23902	0.99661	0.19710
10k - 15k	130,614	0.92729	0.17917	0.92888	0.18578	0.99101	0.14274
15k - 20k	94,331	0.89826	0.14421	0.90415	0.15371	0.98246	0.11189
20k - 25k	73,038	0.86864	0.11991	0.87957	0.13194	0.97051	0.09114
25k - 30k	58,775	0.83801	0.10137	0.85460	0.11110	0.95444	0.07574
30k - 35k	48,710	0.80709	0.08684	0.82967	0.09126	0.93411	0.06394
35k - 40k	41,539	0.77752	0.07555	0.80597	0.07254	0.91056	0.05493
40k - 45k	35,917	0.74781	0.06602	0.78221	0.06258	0.88269	0.04746
45k - 50k	31,528	0.71903	0.05807	0.75920	0.04555	0.85159	0.04132
50k - 55k	27,940	0.69065	0.05120	0.73643	0.03682	0.81698	0.03608
55k - 60k	24,984	0.66303	0.04523	0.71416	0.02142	0.77963	0.03158
60k - 65k	22,444	0.63545	0.03984	0.69178	0.01384	0.73896	0.02756
65k - 70k	20,297	0.60875	0.03508	0.66993	0.00000	0.69667	0.02405
70k - 75k	18,366	0.58154	0.03061	0.64747	0.00000	0.65105	0.02078
75k - 80k	16,696	0.55512	0.02657	0.62541	0.00000	0.60478	0.01787
80k - 85k	15,175	0.52833	0.02275	0.60278	0.00000	0.55647	0.01513
85k - 90k	13,641	0.49826	0.01874	0.57701	0.00000	0.50131	0.01228
90k - 95k	12,083	0.46406	0.01447	0.54716	0.00000	0.43858	0.00928
95k - 00k	10,278	0.41901	0.00923	0.50685	0.00000	0.35817	0.00565

\*1997 Plan credibilities based on 1989 projection year.

## CALIFORNIA EXPERIENCE RATING PLAN COMPARISON OF CREDIBLITIES 1997 Plan vs Projection Year 1991



Primary Credibility





366

## CALIFORNIA EXPERIENCE RATING PLAN COMPARISON OF INDICATED AND 1997 PROMULGATED B & W PLAN 1997 Plan vs Projection Year 1991

	Median		1997 Experien	ce Rating Plan		1991 Iterati	on 2 (Final)
	Exper. Period	Indicated	Values	Promulgat	ed Values	Indicated	d Values
Risks	Expected Loss	В	Ŵ	В	W	В	W
1 - 5k	520,196	8,558	0.381	8,562	0.37	267	0.334
5k - 10k	209,397	9,633	0.249	9,620	0.25	712	0.198
10k - 15k	130,614	10,242	0.193	10,000	0.20	1,185	0.144
15k - 20k	94,331	10,684	0.161	10,000	0.17	1,684	0.114
20k - 25k	73,038	11,045	0.138	10,000	0.15	2,219	0.094
25k - 30k	58,775	11,362	0.121	10,000	0.13	2,805	0.079
30k - 35k	48,710	11,642	0.108	10,000	0.11	3,436	0.068
35k - 40k	41,539	11,886	0.097	10,000	0.09	4,080	0.060
40k - 45k	35,917	12,113	0.088	10,000	0.08	4,773	0.054
45k - 50k	31,528	12,319	0.081	10,000	0.06	5,494	0.049
50k - 55k	27,940	12,514	0.074	10,000	0.05	6,259	0.044
55k - 60k	24,984	12,698	0.068	10,000	0.03	7,062	0.041
60k - 65k	22,444	12,876	0.063	10,000	0.02	7,928	0.037
65k - 70k	20,297	13,045	0.058	10,000	0,00	8,837	0.035
70k - 75k	18,366	13,216	0.053	10,000	0.00	9,844	0.032
75k - 80k	16,696	13,380	0.048	10,000	0.00	10,911	0.030
80k - 85k	15,175	13,547	0.043	10,000	0.00	12,095	0.027
85k - 90k	13,641	13,736	0.038	10,000	0.00	13,570	0.024
90k - 95k	12,083	13,955	0.031	10,000	0.00	15,467	0.021
95k - 00k	10,278	14,251	0.022	10,000	0.00	18,418	0.016

\*1997 Plan credibilities based on 1989 projection year.

367

Exhibit 18

## CALIFORNIA EXPERIENCE RATING PLAN COMPARISON OF INDICATED AND 1997 PROMULGATED B & W PLAN 1997 Plan vs Projection Year 1991



**B** Values

W Values



## CALIFORNIA EXPERIENCE RATING PLAN Experience Rating Formula

Modification = 
$$1 + Z_p \left(\frac{A_p - E_p}{E}\right) + Z_e \left(\frac{A_e - E_e}{E}\right)$$
 Formula 5

From

$$Z_{p} = \frac{E}{E+B}$$
Formula 3  
$$Z_{e} = \frac{E}{E+J_{e}} = \frac{W \cdot E}{E+B}$$
Formula 4

it follows that:

$$1 + Z_{p}\left(\frac{A_{p} - E_{p}}{E}\right) + Z_{e}\left(\frac{A_{e} - Ee}{E}\right)$$

$$= 1 + \left(\frac{E}{E+B}\right) \cdot \left(\frac{A_{p} - Ep}{E}\right) + \left(\frac{E}{E+J_{e}}\right) \cdot \left(\frac{A_{e} - E_{e}}{E}\right)$$

$$= \left(\frac{E+B}{E+B}\right) + \left(\frac{A_{p} - Ep}{E+B}\right) + \left(\frac{A_{e} - E_{e}}{E+J_{e}}\right)$$

$$= \frac{E+B+A_{p} - E_{p}}{E+B} + \frac{A_{e} - E_{e}}{E+J_{e}} \cdot \left(\frac{E+J_{e}}{E+B} \cdot \frac{E+B}{E+J_{e}}\right)$$

$$= \frac{E+B+A_{p} - E_{p} + \left[(A_{e} - E_{e}) \cdot \left(\frac{E+B}{E+J_{e}}\right)\right]}{E+B}$$

$$= \frac{A_{p} + B + \left(\frac{E+B}{E+J_{e}}\right) \cdot A_{e} + \left[(E-E_{p}) - E_{e}\left(\frac{E+B}{E+J_{e}}\right)\right]}{E+B}$$

$$= \frac{A_{p} + B + W \cdot A_{e} + (1-W) \cdot E_{e}}{E+B}$$
Formula 1
where:

$$W = \frac{E+B}{E+J_e} = \frac{Z_e}{Z_p}$$

369

Appendix 1

#### CALIFORNIA EXPERIENCE RATING PLAN EMPIRICAL EXPECTED LOSS RATES AND D-RATIOS Projection Year 1991 5th Report

Clear	Ernlow	n_	Class	Ernlast	D-	Class	Explan	D-	Class	Ero Loss	D-
Code	Rate	Ratio	Code	Rate	Ratio	Code	Rate	Ratio	Code	Rate	Ratio
0005	4 50	0 201	2116	5 4 5	0 271	3085	5.68	0.289	4112	1 23	0 328
0005	4.30	0.301	2110	9.45	0.271	2000	2.65	0.233	4114	5.44	0.310
0010	1.64	0.290	2117	3.07	0.264	3110	5 70	0.333	4130	5.44	0.316
0034	0.46	0.284	2121	3.02	0.300	3110	5.70	0.324	4130	6.10	0.310
0035	4.16	0.280	2142	4.71	0.313	3111	3.05	0.280	4133	5.17	0.272
0036	5.76	0.291	2150	8.09	0.337	3131	3.09	0.526	4150	2.23	0.324
0038	10.79	0.261	2163	4.15	0.317	3146	4.38	0.312	4239	3.56	0.281
0040	3.69	0.305	2211	9.88	0.267	3152	2.42	0.330	4240	4.82	0.312
0041	3.01	0.291	2222	13.79	0.358	3165	4.94	0.276	4243	3.04	0.350
0042	6 58	0.298	2362	8.44	0.311	3169	3.56	0.309	4244	4.93	0.305
0044	4.10	0.309	2402	5.40	0.305	3175	5.13	0.325	4250	4.38	0.334
0046	2 60	0 222	2412	7 97	0.784	2170	2 12	0 224	4753	541	0 308
0043	5.09	0.323	2413	7.02	0.200	3170	2.13	0.324	4170	6 00	0.300
0050	0.29	0.274	2501	3.46	0.327	31/9	5.14	0.327	42/9	J.66	0.239
0079	3.88	0.248	2532	5.05	0.259	3180	0.07	0.318	4283	4.82	0.296
0103	5.36	0.382	2570	7.68	0.308	3220	3.06	0.328	4297	0.62	0.305
0106	15.87	0.221	2571	7.49	0.303	3224	2.15	0.384	4299	3.11	0.331
0171	8.16	0.252	2576	6.52	0.315	3241	6.42	0.320	4304	4.73	0.334
0172	5.80	0.254	2578	7.80	0.307	3255	4.22	0.341	4312	4.77	0.274
0251	3.85	0.304	2585	5.44	0.324	3257	5.00	0.303	4351	0.77	0.415
0400	4.41	0.293	2586	3.60	0.287	3300	5.85	0.379	4354	2.47	0.318
0401	11.06	0.287	2623	13.06	0.322	3339	6.45	0.305	4360	1.15	0.326
	2.62	0.005	2660	0 73	0.292	2266	0.05	0.785	4761	1 79	0 241
1122	3.85	0.225	2000	0.72	0.262	3303	0.03	0.265	4301	1.70	0.341
1123	4.96	0.258	2683	7.89	0.322	33/2	0.38	0.298	4362	1.27	0.278
1124	2.45	0.266	2688	5.98	0.294	3373	4.29	0.353	4410	6.35	0.302
1320	1.89	0.273	2702	12.92	0.226	3383	2.38	0.301	4414	1.66	0.455
1322	10.91	0.240	2710	9.13	0.296	3400	5.82	0.311	4420	10.54	0.297
1330	6.05	0.260	2731	6.14	0.290	3507	6.36	0.303	4431	1.98	0.420
1438	5.95	0.305	2759	7.44	0.305	3574	2.67	0.347	4432	3.78	0.356
1452	2.48	0.275	2790	2.65	0.373	3620	5.74	0.297	4470	5.03	0.293
1463	2 51	0 309	2797	8 70	0 304	3632	3 48	0 322	4478	5 57	0.301
1624	8.65	0.289	2806	8 28	0 312	3643	319	0 323	4511	1.21	0.305
1024	0.05	0.207	2000	0.20	0.012			01020			
1699	2.17	0.339	2812	6.47	0.296	3647	8.67	0.310	4557	3.08	0.335
1701	3.29	0.231	2819	10.49	0.276	3681	1.25	0.322	4558	3.82	0.318
1710	3.28	0.296	2842	8.65	0.283	3686	0.00	1.000	4567	6.30	0.250
1741	3 25	0 307	2881	8.39	0.316	3719	4.27	0.262	4568	3.65	0.188
1803	8.33	0.269	2883	9.23	0.315	3724	5.05	0.278	4611	3.55	0.308
1025	( 22	0.200	2015	0.62	0.766	2776	\$ 22	0 207	4675	2 27	0 225
1925	0.33	0.299	2913	9.02	0.230	3720	5.55	0.297	4035	2.27	0.323
2002	7.60	0.342	2923	4.09	0.355	3805	1.70	0.349	4003	0.24	0.334
2003	4.65	0.308	2960	8.98	0.245	3807	5.81	0.273	4670	5.08	0.339
2014	5.50	0.286	3004	5.70	0.275	3808	1.80	0.436	4683	7.51	0.334
2030	3.91	0.301	3018	2.53	0.249	3815	8.87	0.307	4692	1.40	0.306
2063	3.71	0.334	3022	4.51	0.286	3821	11.12	0.251	4717	2.64	0.378
2081	11.93	0.329	3028	3.25	0.350	3828	6.28	0.317	4720	5.34	0.288
2095	7 58	0 309	3030	9.28	0.269	3830	2.63	0.294	4740	2.37	0.296
2102	4 32	0 330	3040	11.16	0 277	4000	4 53	0.259	4757	2.79	0.324
2106	6.45	0.357	3060	6.26	0.314	4034	8.51	0.277	4771	2.69	0.271
			2011		0.000	40.7.6	2.05	0 202	40.00	4 70	0.214
2107	5.87	0.330	3066	4.52	0.323	4036	3.97	0.282	4828	4.79	0.314
2108	6.22	0.303	3070	1.04	0.346	4038	5.49	0.308	4829	2.29	0.319
2109	6.60	0.323	3076	6.30	0.313	4041	5.70	0.251	4922	1.52	0.360
2111	5.01	0.330	3081	9.10	0.295	4049	4.74	0.311	4983	4.23	0.332
2113	7.55	0.332	3082	3.89	0.341	4111	1.92	0.394	5020	3.39	0.275

#### CALIFORNIA EXPERIENCE RATING PLAN EMPIRICAL EXPECTED LOSS RATES AND D-RATIOS Projection Year 1991 5th Report

Class	Exp Loss	D-	Class	Exp Loss	D-	Class	Exp Loss	D-	Class	Exp Loss	D-
Code	Rate	Ratio	Code	Rate	Ratio	Code	Rate	Ratio	Cede	Rate	Ratio
5022	6.54	0.237	6237	3.27	0.243	7855	5.35	0.259	8350	4.14	0.270
5040	10.09	0.229	6251	7.13	0.279	8001	3.23	0.321	8387	3.96	0.295
5057	13.46	0.221	6252	10.86	0.218	8008	1.72	0.331	8388	5.77	0.294
5059	15.59	0.229	6254	3.15	0.392	8013	1.19	0.292	8389	4.14	0.298
5102	5.91	0.253	6306	4.58	0.242	8015	4.06	0.308	8390	5.80	0.337
5128	1.13	0.341	6319	4.69	0.229	8017	2.62	0.333	8391	3.07	0.314
5146	4.45	0.289	6325	4.85	0.238	8018	4.75	0.310	8392	4.98	0.312
5160	1.70	0.266	6361	4.39	0.250	8021	9.11	0.298	8393	3.64	0.275
5183	4.04	0.288	6364	5.70	0.281	8028	5.03	0.282	8397	5.14	0.294
5184	6.53	0.286	6400	9.24	0.289	8031	4.46	0.325	8400	3.59	0.233
<i>.</i>		0.001				0000				0.00	0.061
5188	4.06	0.261	6504	4.82	0.321	8032	4.37	0.341	8500	9.99	0.251
5190	3.35	0.284	0834	5.27	0.308	8039	2.93	0.368	8601	0.65	0.301
5191	1.85	0.326	7133	2.35	0.315	8041	3.39	0.289	8504	2.37	0.226
5192	3.73	0.342	7198	0.11	0.334	8042	3.22	0.310	8631	11.92	0.261
5200	4.69	0.268	1201	9.55	0.288	8040	2.80	0.331	8/10	8.50	0.303
\$207	6.12	0 379	7710	0 1 4	0.242	80.57	4.06	0.246	9710	1 70	0 222
5207	3.15	0.278	7219	0.14	0.242	8057	4.90	0.240	9720	2.79	0.332
5212	4.11	0.203	7248	2.03	0.117	8059	3.40	0.223	9720	2.80	0.240
5215	3.73	0.251	7272	6.27	0.174	8000	2.93	0.271	0743	0.26	0.210
5214	3.72	0.230	7332	0.39	0.314	8001	3.23	0.260	0741	0.20	0.201
5222	8.79	0.230	/300	9.13	0.273	8002	1.10	0.321	8/42	0.00	0.305
\$775	5 42	0.250	7365	8.04	0.265	8063	2 58	0 306	8745	4 02	0 320
5249	3.42	0.250	7392	7.63	0.200	8064	2.38	0.300	8749	0.84	0.320
5403	6.85	0.200	7302	634	0.299	8065	2 75	0.384	8755	1 36	0.200
5436	6.06	0.240	7403	1.29	0.233	8070	0.00	1 000	8900	3.67	0 3 7 3
5443	A 48	0.200	7405	1.04	0.374	8102	4 44	0.270	8803	0.23	0.321
5445	4.40	0.207	/405	1.04	0.571	0102	4.44	0.270	0005	0.25	0.541
5445	5 27	0 247	7409	5 73	0 193	8103	8 97	0 300	8804	3 74	0 263
5462	7 64	0.283	7410	4.66	0.284	8105	9.00	0.357	8806	4 47	0.341
5473	18.98	0 347	7413	1 4 3	0 385	8106	6 24	0 319	8807	0.50	0 326
5474	6.95	0.235	7419	2 27	0.461	8107	3 54	0.325	8808	0.62	0 317
5479	11.14	0.266	7421	211	0 375	8110	3 29	0.258	8810	0.43	0 322
5477	11.14	0.200	7421	2.11	0.575	0110	5.27	0.200	0010	0.45	0.522
5480	8.16	0.238	7424	2.95	0.319	8111	4.70	0.318	8813	0.52	0.312
5506	4 89	0 262	7426	0.31	0 571	8113	12.25	0 279	8817	0.00	0.551
5507	3.81	0.241	7428	2.14	0.330	8116	4.07	0.307	8818	0.68	0.334
5538	4.80	0.285	7429	12.22	0.333	8117	4.96	0.303	8820	0.41	0.280
5551	17,20	0.205	7500	0.15	0.887	8203	0.00	1.000	8822	0.56	0.337
5606	1.84	0.293	7515	1.72	0.272	8204	18.94	0.227	8823	4.79	0.278
5645	9.78	0.244	7520	3.44	0.288	8209	6.60	0.294	8827	4.49	0.264
5650	6.25	0.266	7538	8.34	0.222	8215	8.69	0.239	8829	6.02	0.290
5703	14.92	0.224	7539	3.57	0.257	8227	3.68	0.270	8830	1.90	0.338
5951	0.65	0.284	7580	2.09	0.303	8232	5.17	0.285	8831	2.92	0.321
						1					
6003	8.99	0.174	7600	1.79	0.310	8264	6.98	0.300	8834	0.91	0.289
6011	7.80	0.215	7601	21.12	0.202	8265	13.27	0.255	8838	1.01	0.313
6204	10.97	0.239	7605	4.05	0.317	8267	7.20	0.265	8839	0.69	0.306
6206	5.62	0.243	7606	7.48	0.308	8278	121.83	0.266	8840	0.59	0.298
6213	3.66	0.200	7610	0.61	0.356	8286	6.64	0.269	8868	1.04	0.309
6216	6.97	0.215	7706	3.97	0.292	8291	5.13	0.295	8875	1.05	0.273
6217	3.73	0.238	7707	1529.26	0.193	8292	9.13	0.282	8901	0.96	0.320
6223	2.15	0.384	7720	6.44	0.278	8293	12.38	0.252	9008	7.45	0.298
6233	4.87	0.238	7721	5.35	0.295	8304	7.37	0.270	9015	5.31	0.270
6235	12.87	0.244	7722	19.83	1.000	8324	5.45	0.285	9016	4.21	0.322

## CALIFORNIA EXPERIENCE RATING PLAN EMPIRICAL EXPECTED LOSS RATES AND D-RATIOS Projection Year 1991 5th Report

9031 4.19 0.284 9085 6.29 0.288 9185 22.57 0.290 9507 3.75 0.301 9048 4.03 0.309 9101 4.97 0.231 9402 5.85 0.247 9322 4.78 0.296 9050 6.03 0.318 9154 2.15 0.340 9403 7.45 0.273 9522 4.78 0.296 9053 2.61 0.325 9156 2.67 0.354 9403 7.45 0.273 9522 9.56 0.210 9060 4.14 0.291 9138 0.00 1.000 9420 5.04 0.232 9.549 5.47 0.297 9066 4.51 0.275 9181 1.39 0.315 9422 4.19 0.288 9549 5.47 0.297 9066 4.51 0.275 9181 1.39 0.315 9422 4.19 0.288 9549 5.47 0.297 9066 0.217 9180 6.20 0.305 9422 4.19 0.288 9549 5.47 0.297 9066 1.2.78 0.323 9180 6.20 0.313 9422 4.19 0.288 9549 5.47 0.297 9066 1.2.78 0.323 9180 6.20 0.313 9422 4.19 0.288 9549 5.47 0.297 9066 1.51 0.277 9181 1.39 0.314 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9020 2.57 0.279	Class Code	Exp Loss Rate	D- Ratio	Ciase Code	Exp Loss Rate	D- Ratie	Class Code	Exp Lose Rate	D- Ratio	Class Code	Exp Loss Rate	D- Ratie
9043 1.80 0.295 9092 3.06 0.303 9220 5.47 0.302 9319 3.47 0.299 9048 403 0.309 9101 4.97 0.281 9403 7.45 0.273 9522 4.78 0.296 9053 2.61 0.325 9156 2.67 0.354 9403 7.45 0.273 9522 9.465 0.210 9060 4.14 0.291 9138 0.00 1.000 9420 5.04 0.232 9.545 1.35 0.350 9061 2.78 0.323 9180 6.20 0.305 9422 4.19 0.298 9549 5.47 0.297 9066 4.51 0.275 9181 1.39 0.313 9424 6.55 0.210 8.18 0.211 9070 5.76 0.279 9182 1.69 0.384 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279	9031	4.19	0.284	9085	6.29	0.288	9185	25.57	0.290	9507	3.75	0.301
9048 4.03 0.309 9101 4.97 0.281 9402 5.85 0.246 9521 4.75 0.260 9050 6.03 0.318 9154 2.15 0.346 9403 7.45 0.273 9522 4.78 0.296 9053 2.61 0.325 9156 2.67 0.354 9410 1.78 0.240 9529 9.65 0.210 9060 4.14 0.291 9158 0.00 1.000 9420 5.04 0.252 9543 1.95 0.350 9061 2.78 0.323 9180 6.20 0.305 9422 4.19 0.298 9545 5.47 0.297 9066 4.51 0.275 9181 11.39 0.315 9424 6.55 0.271 9552 1.081 0.211 9070 5.76 0.279 9182 1.69 0.384 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9182 1.69 0.313 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9456 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9456 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9456 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9456 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9456 8.13 0.221 946 1.53 0.318 9620 2.57 0.279	9043	1.89	0.295	9092	3.06	0.303	9220	5.47	0.302	9519	3.47	0.299
9050 6.03 0.318 9154 2.15 0.340 9403 7.45 0.273 9522 4.78 0.296 9053 2.61 0.325 9156 2.67 0.354 9410 1.78 0.240 9529 9.65 0.210 9060 4.14 0.291 9158 0.00 1.000 9420 5.04 0.252 9549 5.47 0.297 9066 4.51 0.275 9181 11.39 0.315 9424 6.55 0.215 9552 10.81 0.211 9070 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9510 1.53 0.316 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.316 9620 2.57 0.279	9048	4.03	0.309	9101	4.97	0.281	9402	5.85	0.246	9521	4.75	0.260
9053 2.61 0.325 9156 2.67 0.354 9410 1.78 0.240 9529 9.65 0.210 9060 4.14 0.291 9158 0.00 1.000 9420 5.04 0.252 9545 1.53 0.350 9066 4.51 0.275 9181 11.39 0.315 9424 6.55 0.275 9552 1.081 0.211 9070 5.76 0.279 9182 1.69 0.384 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279	9050	6.03	0.318	9154	2.15	0.340	9403	7.45	0.273	9522	4.78	0.296
9060         4.14         0.291         9158         0.00         1.000         9420         5.04         0.232         9545         1.95         0.360           9061         2.78         0.323         9180         6.20         0.305         9422         4.19         0.298         9549         5.47         0.237           9066         4.51         0.275         9181         11.39         0.315         9424         6.53         0.275         9152         10.81         0.211           9079         3.64         0.350         9184         10.20         0.313         9426         8.13         0.221         9586         1.61         0.295           9079         3.64         0.350         9184         10.20         0.313         9501         5.07         0.284         9620         2.57         0.279           9079         3.64         0.350         9184         10.20         0.313         9501         5.07         0.284         9620         2.57         0.279           9620         2.57         0.211         10.20         0.313         951         5.07         0.284         9620         2.57         0.279	9053	2.61	0.325	9156	2.67	0.354	9410	1.78	0.240	9529	9.65	0.210
9061 2.78 0.323 9180 6.20 0.305 9422 4.19 0.238 9549 5.47 0.27 9066 4.51 0.275 9181 11.39 0.315 9424 6.55 0.275 9552 10.81 0.211 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279	9060	4.14	0.291	9158	0.00	1.000	9420	5.04	0.252	9545	1.95	0.350
9066 4.51 0.275 9181 11.39 0.315 9424 6.53 0.275 9552 10.81 0.219 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279 9620 2.57 0.279	9061	2.78	0.323	9180	6.20	0.305	9422	4.19	0.298	9549	5.47	0.297
9070 5.76 0.279 9182 1.69 0.384 9426 8.13 0.221 9586 1.61 0.295 9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279	9066	4.51	0.275	9181	11.39	0.315	9424	6.55	0.275	9552	10.81	0.211
9079 3.64 0.350 9184 10.20 0.313 9501 5.07 0.284 9610 1.53 0.318 9620 2.57 0.279	9070	5.76	0.279	9182	1.69	0.384	9426	8.13	0.221	9586	1.61	0.295
9620 2.57 0.279	9079	3.64	0.350	9184	10.20	0.313	9501	5.07	0.284	9610	1.53	0.318
										9620	2.57	0.279

## CALIFORNIA EXPERIENCE RATING PLAN COMPARISON OF EMPIRICAL AND MANUAL D-RATIOS

	1991	1991		1991	1991
Benchmark	Empirical	Manual	Benchmark	Empirical	Manual
Class	D-	<b>D-</b>	Class	D-	D-
Code	Ratio	Ratio	Code	Ratio	Ratio
0016	0.30	0.32	7198	0.33	0.31
0042	0.30	0.34	7219	0.24	0.31
0172	0.25	0.32	8008	0.33	0.35
2003	0.31	0.33	8017	0.33	0.34
2501	0.33	0.35	8018	0.31	0.33
2883	0.31	0.34	8039	0.37	0.33
3632	0.32	0.33	8232	0.28	0.32
3681	0.32	0.34	8387	0.29	0.31
3830	0.29	0.39	8389	0.30	0.31
4478	0.30	0.32	8391	0.31	0.32
İ					
5183	0.29	0.30	8742	0.31	0.32
5190	0.28	0.31	8810	0.32	0.33
5200	0.27	0.32	8829	0.29	0.38
5213	0.25	0.30	8834	0.29	0.34
5403	0.25	0.30	9008	0.30	0.35
5445	0.25	0.32	9015	0.27	0.32
5474	0.23	0.29	9043	0.29	0.34
5551	0.21	0.28	9050	0.32	0.36
5645	0.24	0.30	9079	0.35	0.35
6217	0.24	0.29			l

## Appendix 4

## CALIFORNIA EXPERIENCE RATING PLAN RIDGE REGRESSION OVERVIEW Hoerl and Kennard's $\delta$

Draper and Smith [4, pp. 318-319] discuss a procedure developed by Hoerl and Kennard which we call Hoerl and Kennard's  $\delta$ . The basic idea is to calculate an initial  $\theta$ ,  $\theta(0)$ , then, using the parameters corresponding to  $\theta(0)$ , calculate the next  $\theta$ . This continues until

Criterion =  $\frac{\theta(j+1)-\theta(j)}{\theta(j)}$  Hoerl and Kennard's  $\delta$ 

where Hoerl and Kennard's  $\delta = 20\{\text{trace}(\mathbf{Z}^*\mathbf{Z})^{-1}/r\}^{-1}^{30}$  and r is the number of parameters in the model. The trace of a matrix is the sum of the elements on the main diagonal. In our experience, this procedure did not work sometimes and in these situations we selected the  $\theta$  corresponding to the minimum criterion. We term the final  $\theta$  the indicated  $\theta$ ,  $\theta(I)$ . The procedure was performed for each group of 5,000. Sometimes the procedure resulted in selection of a  $\theta$  for which Zp is greater than unity. Generally this happened only for the largest risks. As nearly full primary credibility is expected for these risks, this result was deemed to be within a reasonable variance about unity and did not justify rejecting the procedure for this reason alone. Though Hoerl and Kennard's  $\delta$  generally gave a relatively stable pattern of results, the efficiencies were inferior to the Maximum Excess method.

Appendix 5

## CALIFORNIA EXPERIENCE RATING PLAN PARAMETER REFINEMENT

Bias Adjustment Logic for the Quintiles Test Extension

Average is defined as a modification of unity and a standard loss ratio equal to the all risks combined standard loss ratio. Note that a risks modification is always bounded between this empirical modification and unity. Where a risk falls in this range is a function of credibility.

1. Risks with relatively good experience always have modifications less than unity. So,

A) Good experience and a standard loss ratio lower than average
 => that the modification is too high.
 => credibility is too low.

B) Good experience and a standard loss ratio higher than average
 => that the modification is too low.
 => credibility is too high.

2. Risks with relatively poor experience always have modifications greater unity. So,

A) Poor experience and a standard loss ratio lower than average
 => that the modification is too high
 => credibility is too high.

B) Poor experience and a standard loss ratio higher than average
 => that the modification is too low
 => credibility is too low.

If we order risks by their modifications then look at the pattern of the standard loss ratios, we may see:

Modification	Standard Loss Ratios			
< Unity (good experience)	Low	High		
> Unity (poor experience)	High	Low		
Correlation between	Positive	Negative		
modifications and SLRs	(Direct)	(Inverse)		
Implies credibility is	Too Low	Too High		

No pattern implies credibilities are in balance by experience.

Appendix 6

Class			Manu	al D-Ratio	s by Policy	Year			
Code	1998	1995	1991	1990	1989	1985	<u>198</u> 0	1975	1970
0016	0.29	0.32	0.32	0.33	0.34	0.42	0.39	0.40	0.47
0042	0.30	0.32	0.34	0.34	0.35	0.44	0.38	0.42	0.47
0172	0.31	0.32	0.32	0.33	0.33	0.40	0.42	0.38	
2003	0.33	0,34	0.33	0.35	0.36	0.42	0.42	0.42	0.51
2501	0.32	0.33	0.35	0.36	0.38	0.43	0.43	0.42	0.51
2883	0.30	0.31	0.34	0.34	0.36	0.42	0.45	0.41	0.51
3632	0.31	0.31	0,33	0,33	0.34	0.41	0.41	0.40	0.48
3681	0.31	0.31	0.34	0.34	0.36	0.41	0.41	0.37	0.46
3830	0.31	0.35	0.39	0.38	0.36	0.45	0.41	0.43	0.49
4478	0.30	0.34	0.32	0.33	0.35	0.40	0.42	0.41	0.50
5183	0.30	0.31	0.30	0.32	0.34	0.41	0.40	0.37	0.48
5190	0.26	0.28	0.31	0.33	0.34	0.38	0.39	0.38	0.46
5200			0.32	0.34	0.34	0.42	0.43	0.41	0.47
5213	0.30	0.31	0.30	0.31	0.31	0.42	0.40	0.40	0.48
5403	0.28	0.29	0.30	0.32	0.34	0.41	0.40	0.36	0.47
5445			0.32	0.32	0.35	0.42	0.44	0.44	0.50
5474	0.27	0.29	0.29	0.30	0.33	0.36	0.38	0.36	0.46
5551			0.28	0,30	0.31	0.39	0.43	0.35	0.46
5645	0.28	0.29	0.30	0.32	0.34	0.42	0.43	0.41	0.51
6217			0.29	0.31	0.33	0.38	0.39	0.35	0.44
7198	0.30	0.32	0.31	0.32	0.33	0.41	0.45	0.42	0.42
7219	0.30	0.32	0.31	0.32	0.33	0.41	0.41	0.41	0.50
8008	0.32	0.33	0.35	0.34	0.35	0.43	0.39	0.41	0.48
8017	0.31	0.33	0.34	0.34	0.35	0.42	0.40	0.39	0.48
8018	0.31	0.32	0.33	0.34	0.35	0.41	0.42	0.40	0.48
8039	0.35	0.35	0.33	0.33	0.36	0.42	0.39	0.39	0.48
8232	0.29	0.30	0.32	0.31	0.33	0.40	0.39	0.38	0.48
8387	0.31	0.30	0.31	0.32	0.34	0.39	0.40	0.39	0.48
8389	0.30	0.31	0.31	0.30	0.34	0.40	0.40	0.39	0.48
8391	0.30	0.31	0.32	0.33	0.34	0.41	0.42	0.41	0.46
8742	0.30	0.31	0.32	0,32	0.33	0.38	0.38	0.34	0.43
8810	0.32	0.33	0.33	0.34	0.35	0.40	0.41	0.38	0.46
8829	0.33	0.36	0.38	0.37	0.39	0.48	0.44	0.43	0.53
8834	0.33	0.34	0.34	0,35	0.36	0.42	0.41	0.38	0.48
9008	0.31	0.33	0.35	0.37	0.36	0.44	0.42		
9015	0.29	0.30	0.32	0.33	0.33	0.39	0.40	0.39	0.49
9043	0.32	0.33	0.34	0.33	0.35	0.40	0.42	0.38	0.47
9050	0.31	0.33	0.36	0.37	0.38	0.41	0.41	0.39	0.51
9079	0.31	0.33	0.35	0.35	0.36	0.41	0.42	0.41	0.51