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Abstract: The Bornhuetter/Ferguson loss reserving method consists of selecting a development pattern and, for each accident year, an initial ultimate loss ratio. From these, the reserve estimate is derived. In this paper, the usual way to obtain the development pattern from the chain ladder link ratios is criticized because it assumes a multiplicative connection between past and future loss amounts whereas the Bornhuetter/Ferguson method establishes an additive connection (i.e. an independence). Therefore, an alternative approach to derive and select a development pattern is proposed.

Furthermore, the raw data usually contain some implicit information about the underwriting cycle. This paper shows how this information can be extracted from the data and used in the selection of the initial ultimate loss ratios.

Altogether the proposed approach is believed to align with the concepts of Bornhuetter and Ferguson better than the conventional approach does. The result is a standalone reserving method which does not rely upon the use of chain ladder elements.

Keywords. Loss reserving, Bornhuetter/Ferguson, Development pattern, Initial ultimate loss ratio

### 1. Introduction

Let  $C_{i,k}$  denote the cumulative loss amount (either paid or incurred) of accident year *i* after *k* years of development,  $1 \le i$ ,  $k \le n$ , and  $v_i$  be the premium volume of accident year *i*. Then  $C_{i,n+1,i}$  denotes the current loss amount of accident year *i*. Let further  $S_{i,k} = C_{i,k} - C_{i,k,l}$  denote the incremental loss amount (with  $C_{i,0} = 0$ ) and  $U_i$  the (unknown) ultimate loss amount of accident year *i*. For an easier exposition of the ideas, we assume in the beginning that *n* is large enough such that there is no significant loss development beyond development year *n*. We will eliminate this assumption at the end of section 3.

Bornhuetter/Ferguson (BF) introduced their method to estimate  $R_i$  in 1972 in order to cope with a major weakness of the chain ladder (CL) method. Therefore, we will first examine this weakness: The CL uses link ratios  $\hat{f}_k$  in order to project the current loss amount  $C_{i,n+1,i}$  to ultimate, i.e. it estimates  $\hat{U}_i^{CL} = C_{i,n+1-i} \hat{f}_{n+2-i} \cdot \dots \cdot \hat{f}_{n-1} \hat{f}_n$ . Therefore, the CL reserve is

$$\hat{R}_{i}^{CL} = \hat{U}_{i}^{CL} - C_{i,n+1,i} = C_{i,n+1-i} \left( \hat{f}_{n+2-i} \cdot \dots \cdot \hat{f}_{n} - 1 \right).$$

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This means that the reserve is heavily dependent upon the current loss amount  $C_{i,r+1,l}$ . This can lead to a nonsensical reserve  $\hat{R}_{r}^{CL} = 0$  for accident years where currently no claims are paid or reported which is not unusual in excess-of-loss reinsurance for the most recent accident year(s).

The BF method avoids this dependency upon the current loss amount  $C_{i,x+1,r}$ . The indicated BF reserve is defined as

$$\hat{R}_{i}^{BF} := \left(1 - \hat{b}_{n+1-i}\right) \hat{U}_{i}$$

where

 $\hat{U}_i = \nu_i \hat{q}_i$ , with an *a priori* estimate  $\hat{q}_i$  of the ultimate loss ratio (ULR)  $q_i := U_i / \nu_i$  for accident year *i*,

 $b_k \in [0, 1]$  is the percentage of ultimate losses expected to be known after development year k.

Note that  $\hat{q}_i$  is called the *a priori* (or *initial*) estimate of the ULR, in contrast to the posterior estimate  $(C_{i,n+1,i} + \hat{R}_i^{BF})/v_i$  of the ULR. This a priori estimate is different from the posterior estimate if and only if  $C_{i,n+1,i} \neq \hat{b}_{n+1-i}v_i\hat{q}_i$ . The percentages  $(b_1, b_2, ..., b_n)$  constitute the expected cumulative development pattern (with  $b_n = 1$  due to our preliminary assumption regarding *n*) and  $1 - \hat{b}_{n+1-i}$  is therefore the expected outstanding loss percentage of accident year *i*.

Thus, in order to apply the BF method, the actuary has to estimate the parameters q, and  $b_k$  for all i and k. In practice, the  $b_k$  are derived from the CL link ratios in the following way:

$$b_n = 1$$
,  $\hat{b}_{n-1} = \hat{f}_n^{-1}$ ,  $\hat{b}_{n-2} = (\hat{f}_{n-1}\hat{f}_n)^{-1}$ ,...,  $\hat{b}_1 = (\hat{f}_2 \cdot ... \cdot \hat{f}_n)^{-1}$ .

The method itself does not provide an objective approach for the determination of the a priori estimate  $\hat{q}_i$ . In practice, the  $q_i$  are estimated in a variety of ways, often based upon last year's estimate and/or pricing and market information. At worst, this practice can make the estimate  $\hat{q}_i$  appear manipulated in order to achieve a reserve of a desired size. At best, the use of the CL pattern makes it difficult to view the BF method as a standalone reserving method.

Moreover, the use of the CL link ratios assumes that the unknown losses are a direct multiple of the already known losses at each point of the development. This contradicts the basic idea of the independence between  $C_{i,s+1,i}$  and  $\hat{R}_{i}^{BF}$  which was fundamental to the origin of the BF method.

Therefore, this paper develops an alternative approach to estimating the BF parameters  $q_i$  and  $b_k$  without the use of CL concepts along with rather clear guidance on how to arrive at an a priori estimate for the ultimate loss ratio  $q_i$ . Through this approach, the BF method becomes a true alternative to the CL method.

## 2. Estimation of the Development Pattern

If we already have an a priori estimate for  $U_i$  (e.g. from the traditional approach as outlined above), we are able to estimate the appropriate development pattern. From the BF reserve formula  $\hat{R}_i^{BF} = (1 - \hat{b}_{i+1-i}) \hat{U}_i$  we deduce

$$\hat{b}_{u+1-i} = 1 - \frac{\hat{R}_i}{\hat{U}_i} = \frac{\hat{U}_i - \hat{R}_i}{\hat{U}_i} \approx \frac{C_{i,u+1-i}}{\hat{U}_i}$$

As previously stated, the  $\approx$ -sign is a strict equality only if the a priori estimate  $\hat{U}_i$ , equals the posterior  $C_{i,n+1,i} + \hat{R}_i$ , i.e. if  $C_{i,n+1-i} = \hat{b}_{n+1-i}\hat{U}_i$ . This will not be the case for every *i* but should be true on average, at least approximately, otherwise the pattern  $\hat{b}_1, \hat{b}_2, \dots$  would not fit to the data. Therefore, the previous approximate equation suggests the estimator

$$\hat{b}_{k} := \sum_{i=1}^{n+1-k} C_{ik} / \sum_{i=1}^{n+1-k} \hat{U}_{i}$$

as weighted average of the ratios  $C_{i,k}/\hat{U}_r$ . This direct way of estimating the cumulative pattern  $b_1$ ,  $b_2$ , ... may lead to inversions, i.e.  $\hat{b}_k > \hat{b}_{k+1}$ , because each  $\hat{b}_k$  is based on a different number of accident years. In order to avoid such inversions, we use the corresponding increments

$$\hat{\beta}_{k} := \sum_{j=1}^{n+1-k} S_{ik} / \sum_{j=1}^{n+1-k} \hat{U}_{j}$$

and obtain  $\hat{b}_k$  by adding up the  $\hat{\beta}_k$ , i.e. take

$$\hat{b}_k = \hat{\beta}_1 + \dots + \hat{\beta}_k$$

and supplement it with  $\hat{b}_{s+1} = 1$ .

This is the development pattern as suggested by the BF reserve formula itself. This pattern is different from the CL pattern as can be seen e.g. from the numerical example below. Of course, the  $\hat{\beta}_{k}$  should be smoothed and decreasing towards 0. This can be achieved by smoothing selections much as one would do when selecting CL link ratios. We will apply such a procedure together with the estimation of the ultimate loss ratio in the next section. But the actuary who wants to stay with the traditional BF way to arrive at an estimate for  $U_{i}$  can stop reading here and just use the specific BF pattern derived above.

#### 3. Estimation of the Initial Ultimate Loss Ratios

As said in the introduction, the BF method aims at developing an estimate for  $q_i$ , which does not directly depend on the losses  $C_{i,n+1,i}$  known to-date and can be similarly obtained by another actuary. The procedure proposed here employs a three-steps approach. The first step considers the average incremental loss ratio (ILR)

$$\hat{m}_k := \sum_{i=1}^{n+1-k} S_{ik} \bigg/ \sum_{i=1}^{n+1-k} v_i$$

of development year k observed to-date. The sum  $\hat{m}_i + ... + \hat{m}_n$  of all average ILRs is an a priori estimate of the ultimate loss ratio of an average accident year (if the development is assumed to be finished after *n* years). Note that in determining this a priori estimate, the known loss experience  $C_{i,n+1,i}$  of any fixed accident year *i* is taken into account only marginally (as opposed to the CL estimate for  $U_i$ ).

In the second step, we leverage the fact that the ultimate loss ratio  $q_i$  of accident year i is highly influenced by the level of the rate adequacy of that particular year. The rate adequacy is determined by two factors: the rate level and the loss level, which together yield the level of the loss ratio. But whereas in rate making we have to determine a sufficient absolute rate level – sufficient to pay all costs of the business -, for reserving purposes it is sufficient to judge the relative level of rate adequacy of an accident year as compared to the other accident years. With this information we can translate the (almost) known loss ratio of the oldest accident year(s) into predictions for the more recent accident years. Thus, we have to estimate the rate level change and the loss cost trend only. This is much easier because, at the time of reserving, we know the degree to which any rate changes have been realized and we know already some part of the losses of each accident year. This information should therefore be used for the assessment of the rate adequacy in addition to the information from the time of rate making.

Thus, we analyze what the run-off data tell us about the rate adequacy. If an accident year i has a below average rate adequacy (as compared to the other accident years considered), then the premium volume  $v_i$  is smaller than it should be for an average accident year. Therefore, most of its observed individual incremental loss ratios

$$\frac{S_{i,1}}{v_i}, \frac{S_{i,2}}{v_i}, ..., \frac{S_{i,n+1-i}}{v_i}$$

will be higher than the corresponding averages

$$\hat{m}_1, \ \hat{m}_2, \ \dots, \ \hat{m}_{n+1-n},$$

at least after we have eliminated any unusually large individual losses as is normally done with any loss reserving method. In order to arrive at a single figure indicating the emerged relative rate adequacy level of accident year *i* (as compared to the average level of all accident years considered) we use the weighted average

$$r_{i} := \sum_{k=1}^{s+1-r} \frac{\hat{m}_{k}}{\sum \hat{m}_{j}} \cdot \frac{S_{ik} / v_{i}}{\hat{m}_{k}} = \sum_{k=1}^{s+1-r} S_{ik} / \sum_{k=1}^{s+1-r} \left( v_{i} \hat{m}_{k} \right) = \frac{C_{i,s+1-r} / v_{i}}{\sum_{k=1}^{s+1-r} \hat{m}_{k}}$$

of the ratios of  $S_{i,k}/v$ , and  $\hat{m}_k$ . Thus,  $r_i$  is the ratio of the current individual loss ratio  $C_{i,k+1,i}/v_i$  of accident year *i* divided by the corresponding a priori average loss ratio. Therefore,  $r_i$  can be called a *loss ratio index*.

As seen from the premium perspective,  $r_i$  indicates the factor by which the premium  $v_i$  has to be multiplied in order to adjust it to the average rate adequacy level of the accident years i = 1, ..., n considered. From this perspective,  $r_i$  can be called an *on-level premium factor*. Again, the factor  $r_i$  does not necessarily bring the premium  $v_i$  to the sufficient absolute size; it only achieves that – in relation to  $v_i$ , instead of  $v_i$  - all accident years have approximately the same ultimate loss ratio  $U_i/(v_i r_i) \approx \hat{m}_i + ... + \hat{m}_u$ , may the latter be profitable or not. At this stage we can already state that, if the  $r_i$ 's and the  $\hat{m}_i$ 's are plausible, then

$$(\hat{m}_{1} + ... + \hat{m}_{n})r_{1}$$

is a reasonable a priori estimate of the ultimate loss ratio  $q_i = U_i/\nu_i$  (if the development is assumed to be finished after *n* years).

As a third step, we have to check the plausibility of  $r_r$ . Initially we realize that the paid data and the incurred data will yield different values for  $r_r$ . But of course, these should be identical because they relate to the same premium  $v_r$  and losses  $U_r$  for either set of data. Without additional knowledge, we would therefore use the straight average  $(r_i^{puid} + r_i^{mr})/2$  or – as we deal with factors - rather the geometric mean

$$\overline{r_i} = \sqrt{r_i^{puid} \cdot r_i^{mic}} \; . \label{eq:r_i}$$

The calculation of the  $r_i$ 's should be based on the data of a rather large portfolio in order to have the factors  $r_i$  be as reliable as possible. This large portfolio could be comprised of several run-off triangles for which the reserving is done separately, but which are assumed to have undergone similar changes in rate adequacy level.

Normally, we also have some information from pricing available, i.e. the rate changes effected and an estimate of the loss trend. The ratio  $r_i/r_{i,i}$  of any two consecutive years should be checked against the ratio of the loss trend and the effective rate change imbedded in  $v_i$  (in combination these represent the indicated change of the rate adequacy level). For instance, if from year *i*-1 to year *i* a loss increase of +10% is expected but a rate change of only +5% has been achieved, the ratio  $r_i/r_{i-1}$  should be close to 1.10/1.05 indicating a deterioration of the loss ratio by 4.8% (= 1.10/1.05 - 1). If not, we have to make a decision between these two ratios, e.g. form a credibility-weighted average of both values.

For the most recent accident years i=n and i=n-1 we probably will trust the pricing information more than the  $r_r$ -estimate from the data, as the latter only relies on one or two entries in the triangle. At an extreme,  $r_i$  could be 0, which would be nonsensical and must obviously be adjusted. The size of  $r_i$  for the first accident year can in principle be chosen arbitrarily, because its rate adequacy level (loss ratio level) will be taken into account in a subsequent adjustment of  $\hat{m}_k$ , see below. Therefore it can be left as it comes out of the formula in order to keep the  $\hat{m}_k$  at the intuitive incremental loss ratio level.

What really matters are the relativities  $r_i/r_{r,i}$ . Therefore, we first select the values for these relativities based on all information available and then, starting with a selection for  $r_i^*$ , derive from these the resulting selections  $r_i^*$  for each accident year *i*. With these selected  $r_i^*$ , all adjusted premium volume figures  $v_i r_i^*$ ,  $1 \le i \le n$ , should ultimately lead to (approximately) the same rate adequacy level, i.e. yield similar values of  $U_i/(v_i r_i)$ .

At next year's reserve calculation, the data triangle will contain an additional diagonal which will result in changes to all  $r_i$ . But the ratios  $r_i/r_{i,1}$  have the same interpretation as before. Therefore, due to the arbitrariness of  $r_i^*$ , we can keep the "old"  $r_i^*$  and – as long as no changes in

the ratios  $r_{i+1}^*/r_{i+1}^*$  are indicated – also keep the other  $r_i^*$  and just add a new  $r_{n+1}^*$  based on a plausible ratio  $r_{n+1}^*/r_n^*$ .

Before using  $r_i^*$  for the estimation of q, we have to adjust the average incremental loss ratios  $\hat{m}_k$  because these were based on the unadjusted premium volume figures  $v_r$ . Therefore we replace  $\hat{m}_k$  with

$$\hat{\tilde{m}}_{k} := \sum_{i=1}^{n+1-k} S_{ik} / \sum_{i=1}^{n+1-k} (v_{i}r_{i}^{*}).$$

Often this will result in minor changes only. Major changes may happen for the last two or three development years or generally with data where the sizes of  $v_i$  or  $r_i^*$  vary significantly.

The adjusted ILRs  $\hat{\vec{m}}_{k}$  of the last few development years could still produce unintuitive results, again due to the limited number of data points. Of course, these incremental values should be smooth and decreasing towards 0. Therefore, a smoothing approach is reasonable, and we denote the ILRs finally selected with  $\hat{m}_{k}^{*}$ .

At this point we will abandon the unrealistic assumption of not having any development beyond development year *n*. This is simply achieved by selecting an average tail ratio  $\hat{m}_{n+1}^*$  (which may be 0 or even negative, like any other  $\hat{m}_k^*$ ), to supplement the ILRs  $\hat{m}_k^*$ ,  $1 \le k \le n$ , already selected.

Using these selected ILRs, we now have

$$\hat{m}^* := \hat{m}_1^* + ... + \hat{m}_n^* + \hat{m}_{n+1}^*$$

as an adjusted estimate for the ULR at average rate adequacy level. Of course, the paid data should have the same estimated ULR  $\hat{m}^*$  as the incurred data. If that is not the case, we must adjust some  $\hat{m}_k^*$ , especially  $\hat{m}_{n+i}^*$ , to achieve the equality  $\hat{m}_{paid}^* = \hat{m}_{int}^*$ . This finally yields the a priori estimate  $\hat{q}_i := r_i^* \hat{m}^*$  for the ULR of accident year *i* and the corresponding amount  $\hat{U}_i := v_i r_i^* \hat{m}^*$ .

In contrast to the traditional BF procedure, this procedure gives the actuary the possibility to consolidate the general pricing and market information available with the trends and relativities contained in the paid and incurred data triangle. Moreover, this procedure uses a detailed decomposition of the initial ultimate loss ratio  $\hat{q}_i = r_i^*(\hat{m}_1^* + ... + \hat{m}_{u+1}^*)$  into its components rate

adequacy and development pattern. This makes the procedure easier to be followed or peerreviewed by any other actuary.

## 4. Estimation of the Development Pattern (continued)

Now, we insert the result  $\hat{U}_i = v_i r_i^* \hat{m}^*$  of the previous section into the formula derived for  $\hat{\beta}_k$  in section 2 and obtain

$$\hat{\beta}_{k} = \frac{\sum_{i=1}^{n+1-k} S_{ik}}{\sum_{i=1}^{n+1-k} \hat{U}_{i}} = \frac{\sum_{i=1}^{n+1-k} S_{ik}}{\sum_{i=1}^{n+1-k} v_{i} r_{i}^{*} \hat{m}^{*}} = \frac{\hat{m}_{k}}{\hat{m}^{*}}$$

Here we see that the numerator  $\hat{\vec{m}}_k$  may differ from the finally selected  $\hat{\vec{m}}_k$ , as the denominator reflects the selected ILRs. Therefore it is logical to select

$$\hat{\beta}_k^* := \frac{\hat{m}_k^*}{\hat{m}^*}.$$

This finally leads to

$$\hat{b}_{k}^{*} := \hat{\beta}_{1}^{*} + ... + \hat{\beta}_{k}^{*} = \frac{\hat{m}_{1}^{*} + ... + \hat{m}_{k}^{*}}{\hat{m}_{1}^{*} + ... + \hat{m}_{n+1}^{*}}.$$

This is the genuine BF development pattern which is different from the CL pattern (see the numerical example below).

## 5. Putting it all Together

Altogether, we have the following steps of calculation:

$$\begin{split} \hat{m}_{k} &= \sum_{i=1}^{n+i-k} S_{ik} / \sum_{i=1}^{n+i-k} v_{i} & \text{raw incremental loss ratio (ILR) at development year } k \\ r_{i} &= \sum_{k=i}^{n+i-i} S_{ik} / \sum_{k=i}^{n+i-i} (v_{i} \hat{m}_{k}) & \text{raw on-level premium factor for accident year } i \\ r_{i}^{*} &= \text{selected on-level premium factor for accident year } i \text{ (same for paid and incurred)} \\ \hat{m}_{k}^{*} &= \text{selected average ILR at development year } k \\ & (\text{smoothed version of } \hat{\bar{m}}_{k} = \sum_{i=i}^{n+i-k} S_{ik} / \sum_{i=i}^{n+i-k} (v_{i} r_{i}^{*})) \\ \hat{q}_{i} &= r_{i}^{*} \left( \hat{m}_{i}^{*} + ... + \hat{m}_{n}^{*} + \hat{m}_{n+i}^{*} \right) & a \text{ priori ULR for accident year } i, \text{ including tail ratio } \hat{m}_{n+i}^{*} \end{split}$$

$$\hat{U}_i = v_i \hat{q}_i = v_i r_i^* \left( \hat{m}_i^* + ... + \hat{m}_{n+1}^* \right) \quad a \text{ priori} \text{ estimate of ultimate losses for accident year } i$$

$$\hat{b}_{k}^{*} = \frac{\hat{m}_{1}^{*} + ... + \hat{m}_{k}^{*}}{\hat{m}_{1}^{*} + ... + \hat{m}_{n+1}^{*}} \quad \text{avg. cumulative percentage paid (incurred) at development year } k$$

$$\hat{R}_i = (1 - \hat{b}_{n+1-i}^*) \hat{U}_i = \nu_i r_i^* (\hat{m}_{n+2-i}^* + \dots + \hat{m}_{n+1}^*) \quad \text{loss reserve for accident year } i$$

With this way of estimating its parameters  $q_i$  and  $b_k$ , the BF method is truly a standalone reserving method which is completely independent of the CL method. As shown in section 2, this way of calculating the pattern  $b_1$ ,  $b_2$ , ... can also be used if the a priori estimates  $\hat{q}_i$  and  $\hat{U}_i = v_i \hat{q}_i$  are arrived at in a different (e.g. traditional) way. Thus, even if one does not like to work with  $m_k$  and  $r_p$  one should at least adopt the estimation of the pattern as outlined above and avoid using the CL pattern.

### 6. Numerical Example

Data from General Liability Excess business are used to demonstrate the method. Exhibit A contains the premiums  $v_i$  and the incremental amounts  $S_{i,k}$  of the incurred and the paid losses for the accident years 1992 – 2004 and development years 1 to 13. Some negative amounts have been kept in order to demonstrate that this does not lead to distortions. Exhibits B and C show the detailed results of the calculations for the incurred and the paid data respectively. These two exhibits are subdivided into three column blocks and two row blocks indicating the order of calculation: Columns (A) through (C) and rows (1) through (2) are the given data in aggregated form. From these the various components are calculated in the following order:

Columns (D) through (G),

Rows (5) through (9),

Columns (H) through (M).

In the headings of column (H) and row (9), (8#) stands for the last number in row (8), i.e.  $\hat{m}^*$ . The suffix  $_{+k}$  in rows (2), (3) and (5) stands for summation over *i*, i.e.  $\sum_{i=1}^{n+1-k}$ , The term "post." in columns (L) and (M) stands for "posterior". The bold headings  $\mathbf{r}_i^*$ ,  $\mathbf{m}_k^*$  and **Tail-ILR** indicate those positions where selections were required. These selections have been made in the following way:

Rows (3) through (4),

Before selecting  $\mathbf{r}_i^*$  we looked at Exhibit D where the raw  $\mathbf{r}_i$  from column (E) are plotted for both paid and incurred data. The graph shows that the two sets of data are reasonably consistent, except for accident year 2004. Therefore, for i = 1992, ..., 2002, we selected  $\mathbf{r}_i^*$  as the geometric mean between the paid  $\mathbf{r}_i$  and the incurred  $\mathbf{r}_i$ . For i = 2003 and 2004, we have set  $\mathbf{r}_i^* = 0.50$  for both, incurred and paid. The latter choice is not based on any further information. It is just an example. As mentioned earlier, information from pricing should also be used when making the selection. But even without this, the resulting  $\mathbf{r}_i^*$  seem to give a realistic picture of the rather extreme rate adequacy level changes over the years considered. These  $\mathbf{r}_i^*$  correspond to the following adequacy changes:

i-1→i	92→93	93→94	94→95	95→96	96>97	97→98	98→99	99 <del>-→</del> 00	00→01	01→02	02→03	03→04
t <sub>i</sub> */t <sub>i-1</sub> *	0.89	0.95	().94	1.52	1.49	1.26	1.54	0.72	0.66	0.79	0.67	1.00

If we interpret r, a loss ratio index, the above figures imply that we assume a decrease of the loss ratio index  $r_i$  from 1992 to 1993 of 11% (= 0.89 - 1) and an increase of 52% from 1995 to 1996.

 $\mathbf{m_k}^*$  has been taken from row (6) ( $\mathbf{m_k}^\circ$ ) for development years  $\mathbf{k} = 1, ..., 7$ . All the other  $\mathbf{m_k}^*$  have been selected in order to make the development smoothly decreasing. Of course, other selections would have been possible. The **Tail-ILR** for incurred has been selected to be 0 and the **Tail-ILR** for paid has been selected such that the sum  $\hat{m}^*$  of all paid ILRs equals that of the incurred-ILRs which is 137.9%. Note that the traditional way to apply BF will yield exactly the same reserve  $\mathbf{R}_i$  as obtained in column (K) if we use  $1.379 \cdot \mathbf{r}_i^*$  as initial loss ratio and the pattern from row (9).

Finally, Exhibit E shows a comparison between the raw development pattern as proposed here and the pattern derived from the raw CL factors. More precisely, the BF pattern is a plot of  $\hat{b}_{k}^{nnv} = \frac{\hat{m}_{i} + ... + \hat{m}_{k}}{\hat{m}_{i} + ... + \hat{m}_{k}}$  using the raw ILR's  $m_{k}$  of row (4), whereas the CL pattern is a plot of  $\hat{b}_{k}^{CL} = (\hat{f}_{k+1} \cdot ... \cdot \hat{f}_{n})^{-1}$  with  $\hat{f}_{k} = \sum_{i=1}^{n-k} C_{i,k+1} / \sum_{i=1}^{n-k} C_{i,k}$ . We see that the raw BF pattern is clearly different from the raw CL pattern for either data set.

## 7. Final Remarks

As with any reserving method, this approach to estimating the parameters (i.e. the reserve) relies on implicit assumptions. One main assumption has already been addressed in the beginning: the data observed to-date and the amounts still outstanding are independent. This assumption is a cornerstone of the BF method. As the assumption should hold at any point in time, it essentially means that all incremental amounts  $S_{i,1}, \ldots, S_{i,n}$  of each accident year are assumed to be independent. This would be violated if claim payments or bookings of case reserves were not done in the same way each year, especially if high payments in one calendar year would be followed by rather delayed payments in the following year(s). Similarly, the independence of the accident years is implicitly assumed in the estimation of  $m_k$ . This independence assumption is normally less problematic but could also be violated by calendar year effects. A more critical assumption is that the development pattern is consistent across all accident years. Of course, this assumption is not unique to this approach, as it is also implicit in the traditional BF method, as well as in the CL. This assumption should be especially borne in mind when selecting the accident years upon which the parameter estimates are to be based.

The way in which the parameters  $r_i$  and  $m_k$  are estimated consists of starting with an estimate for  $m_k$  which then is used to estimate  $r_r$ . The latter is adjusted and then used to arrive at an improved estimate for  $m_k$ . Thus, it may be tempting to again use this improved estimate of  $m_k$  to improve the estimate for  $r_i$ . But one must be cautious here. External judgment has already been applied in developing these parameters, and therefore any further changes based on the run-off data would only serve to dilute the (presumably desired) impacts of those judgments. Similarly, a purist might be tempted to iterate the estimations without any adjustments in between, i.e. to start with  $\hat{m}_k$  and  $r_i$  as given in section 4, and with  $\hat{\tilde{m}}_k$  as in section 3, but then to use the latter for calculating  $\tilde{r}_i = \sum_{k=1}^{s+1-i} S_{ik} / \sum_{k=1}^{s+1-i} (v_i \tilde{\tilde{m}}_k)$ . This would then be iterated by calculating new estimates, first for  $m_k$  then for  $r_i$  by using the corresponding estimates obtained immediately before. Indeed, this procedure will quickly converge upon and yield exactly the same reserves as the CL does (for a full triangle only). This is not surprising, since proceeding in this way implies that we fully believe all the information contained in the data, without any input of external information. Thus we see that the input of external information is vital for the BF method.

For the CL, a methodology of assessing the variability of the reserves has been established in recent years. See e.g. the papers by Murphy or Mack in the 1994 CAS Spring Forum. Therefore, one would like to have this for BF, as well. For this purpose, we refer to the fact that our way of modeling the BF method can be seen as a cross-classified model, as in automobile rating, based upon the assumption  $E(S_{ik}/v_i) = r_{ik}$ . Thus it can be treated using Generalized Linear Models.

However, this would use the "wrong" volume  $v_i$  instead of  $v_{fr}$ . Moreover, an appropriate assumption for the variance is necessary, too. Therefore, it may seem easier to use the alternative approach of embedding this BF model into the classical credibility IBNR model (see the author's paper "Improved Estimation of IBNR Claims by Credibility Theory" in the journal *Insurance: Mathematics & Economics* of 1990). In this way, the rate level  $r_i$  would be treated as a random variable. In any case, the issue of reserve variability deserves a separate paper.

## 8. References

Bornhuetter, Ronald L. and Ronald E. Ferguson, "The Actuary and IBNR", 1972 PCAS.

Mack, Thomas, "Improved Estimation of IBNR Claims by Credibility Theory", Insurance: Mathematics & Economics 1990.

Mack, Thomas, "Measuring the Variability of Chain Ladder Reserve Estimates", 1994 CAS Spring Forum, Vol. 1. Murphy, Daniel M., "Unbiased Loss Development Factors", 1994 CAS Spring Forum, Vol. 1, and 1994 PCAS.

#### Abbreviations

BF: Bornhuetter/Ferguson

CL: chain ladder

ILR: incremental loss ratio ULR: ultimate loss ratio

### About the author

The author is retired (since 2006) chief actuary non-life of Munich Re. He studied Mathematics at the universities of Munich and Mannheim (Germany) and then worked more than 30 years for Munich Re. He is a member of the German Actuarial Association and a honorary member of the Institute of Actuaries (UK) and of the SAV (Switzerland). He has written several papers, mainly published in the ASTIN Bulletin. He has been awarded the 2<sup>nd</sup>-3<sup>rd</sup> prize at the CAS prize paper competition on variability of loss reserves in 1992 and the Charles A. Hachemeister prize in 1994.

				111CU 1.085 /	mounts										
Acc. Year	Premium	Dev.Yr.	1	2	3	4	5	6	7	8	9	10	11	12	13
19	92 4102	0 7	362	3981	4881	5080	3806	2523	792	731	-1	241	247		
19	93 5754	7 5	i400	7208	7252	4946	4394	3198	3039	-771	-1	-495	-347 -182	3	-115
19	94 6094	0 2	215	12914	6494	5585	2211	3363	2126	445	421	-495		1251	
19	95 6303	4 1	109	6581	5833	4827	5672	8638	12	146	44)54		849		
19	96 6125	6 (	220	10065	10343	11259	9032	1207	26	4221	378	-625			
19	97 5723	1 1	324	6579	16428	17453	20457	3209	7103	101	516				
19	98 9113	7 5	772	12714	22918	33920	20709	33941	28483	101					
19	99 9692	58	563	47206,	59695	60043	50458	5129	-0100						
20	00 16702	1 11	771	48696	84750	77361	39404								
20	01 14849	4 11	259	27000	38648	51890									
20	02 16541	0 11	855	27183	25927										
20		9 6	236	18214											
20	04 22645	47	818												
		Increme	ntal Paid	Loss Amou	unts										
Acc.Year	Premium	Increme Dev.Yr.		Loss Amou 2	ants 3	4	5	6	7	8	9	10	11	12	13
199	92 4102	Dev.Yr.				4 3530	5 6539								
199 199	02 41020 03 5754	Dev.Yr.	1	2	3			2737	2546	1815	335	110	18	26	13 -1
199 199 199	02 4102 03 5754 04 6094	Dev.Yr. ) 7 1	1 234	2 4643	3 6249	3530	6539		2546 5110	1815 611	335 776	110 409	18 48		
199 199 199 199	02 41020 03 5754 04 60940 05 6303	Dev.Yr. ) 7 1 )	1 234 994	2 4643 4936	3 6249 4825	3530 6180	6539 7659	2737 1951	2546	1815 611 1440	335 776 1283	110 409 67	18	26	
199 199 199 199 199	02         41020           03         5754'           04         60940           05         6303-           06         61250	Dev.Yr. ) 7 1 ) 4	1 234 994 -75	2 4643 4936 3208	3 6249 4825 7853	3530 6180 7127	6539 7659 5360	2737 1951 3876	2546 5110 3426	1815 611	335 776 1283 3244	110 409	18 48	26	
199 199 199 199 199 199	22         41020           23         5754'           04         60940           05         6303-           06         61250           07         57231	Dev.Yr. ) 7 1 ) 4 5 -	1 234 994 -75 236 976 730	2 4643 4936 3208 2202	3 6249 4825 7853 4125	3530 6180 7127 5003	6539 7659 5360 4189	2737 1951 3876 9064	2546 5110 3426 2202	1815 611 1440 2064	335 776 1283	110 409 67	18 48	26	
199 199 199 199 199 199 199	02         41020           03         5754'           04         60944           05         6303-           06         61256           07         57231           08         91137	Dev.Yr. ) 7 1 ) 4 5 - 7	1 234 994 -75 236 976 730 539	2 4643 4936 3208 2202 4719	3 6249 4825 7853 4125 9397	3530 6180 7127 5003 13253	6539 7659 5360 4189 6106	2737 1951 3876 9064 4975	2546 5110 3426 2202 3049	1815 611 1440 2064 4719	335 776 1283 3244	110 409 67	18 48	26	
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199 199 199 199 199 199 199 199 200 200	22         41020           33         5754'           460944         60944           95         6303-           66         6125-           77         57231           88         91137           99         96922           90         167021           91         148494	Dev.Yr. 7 1 9 4 5 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 234 994 -75 236 976 730 539 725 312 988	2 4643 4936 3208 2202 4719 3353 5238 14900 6442 9921	3 6249 4825 7853 4125 9397 12904 14901 34676	3530 6180 7127 5003 13253 10642 24865 43595	6539 7659 5360 4189 6106 16491 20274 52621	2737 1951 3876 9064 4975 8886 17769	2546 5110 3426 2202 3049 7228	1815 611 1440 2064 4719	335 776 1283 3244	110 409 67	18 48	26	
199 199 199 199 199 199 199 200 200 200	22         4102           33         5754'           34         6094           35         6303           36         6125           37         5723:           38         9113'           99         9692:           30         16702!           30         14849           31         14849           32         16541(	Dev.Yr. ) 7 1 4 5 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - - - - - - - - - - - - -	1 234 994 -75 236 976 730 730 739 725 312 2088 260	2 4643 4936 3208 2202 4719 3353 5238 14900 6442 9921 7181	3 6249 4425 7853 4125 9397 12904 14901 34676 43596	3530 6180 7127 5003 13253 10642 24865 43595 88702	6539 7659 5360 4189 6106 16491 20274 52621	2737 1951 3876 9064 4975 8886 17769	2546 5110 3426 2202 3049 7228	1815 611 1440 2064 4719	335 776 1283 3244	110 409 67	18 48	26	
199 199 199 199 199 199 199 199 200 200	22         41024           33         5754'           34         60944           35         6303-           36         61254           37         57233           38         91137           39         96922           300         167021           301         148492           32         165416	Dev.Yr. ) 7 1 ) 4 5 1 - 7 5 1 2 9	1 234 994 -75 236 976 730 539 725 312 988	2 4643 4936 3208 2202 4719 3353 5238 14900 6442 9921	3 6249 4825 7853 4125 9397 12904 14901 34676 43596 20357	3530 6180 7127 5003 13253 10642 24865 43595 88702	6539 7659 5360 4189 6106 16491 20274 52621	2737 1951 3876 9064 4975 8886 17769	2546 5110 3426 2202 3049 7228	1815 611 1440 2064 4719	335 776 1283 3244	110 409 67	18 48	26	

#### **Incremental Incurred Loss Amounts**

Parameter
Estimation
Parameter Estimation for Bornbuetter/
/Ferguson

Exhibit B

	(M)	(I.)	(K)	0)	(1)	(11)		(G)	(ŀ)	(E)	(D)		(C)	(B)	(^)
	post. ULR	post. U,	R,	1-b <sub>n+1-i</sub>	Ui	4		v,r,*	ri*	г,	Σm <sub>k</sub>		Cin+1-i	vi	Acc. Year i
	(1.)/(13)	(C)+(K)	()*(J)	from (9)	(B)*(H)	(1)*(8#)		(B)*(ŀ)	selected	C)/(B)/(D)	from (4) (				
,	70.5°%	28,937.0	0.0	0.0%	32,299.9	78.7%		23,421.1	0.57	0.53	132.6%		28,937	41,020	1992
	63.0° a	36,257.2	29.2	0.1%	40,279.1	70,0%		29,206.9	0.51	0.47	132.9%		36,228	57,547	1993
	60.4° 'n	36,829.4	88.4	0.2%	40,634.6	66.7%		29,464.7	0.48	0.46	131.6%		36,741	60,940	1994
,	57.9%	36,476.7	229.7	0.6%	39,604.3	62.8%		28,717.6	0.46	0.44	131.4°%		36,247	63,034	1995
	87.4%	53,513.8	762.8	1.3%	58,440.6	95.4° o		42,376.1	0.69	0.65	131.8%		52,751	61,256	1996
	130.9%	74,895.5	2,241.5	2.8%	81,346.9	142.1%		58,985.8	1.03	0.98	129.7%		72,654	57,231	1997
	185.3°%	168,874.5	10,417.5	6.4%	163,258.7	179.1%		118,381.1	1.30	1.36	128.3°%		158,457	91,137	1998
	281.3%	272,663.7	41,569.7	15.5°%	268,150.6	276.7%		194,439.7	2.01	2.01	118.7%		231,094	96,925	1999
	204.5°%	341,491.4	79,509.4	24.0%	331,893.1	198.7%		240,660.2	1.44	1.46	107.1%		261,982	167,021	2000
	137.2° o	203,774.1	74,977.1	38.7%	193,519.8	130.3%		140,323.8	0.94	1.02	84.7° o		128,797	148,494	2001
	101.3%	167,621.5	102,656.5	60.5%	169,559.7	102.5%		122,950.0	0.74	0.75	52.4° .		64,965	165,410	2002
	66.2%	151,140.1	126,690.1	80.5°%	157,381.6	69.0%		114,119.5	0.50	0.44	24.4%		24,450	228,239	2003
	68.9%	156,136.1	148,318.1	95.0%	156,150.7	69.0%		113,227.0	0.50	0.58	5.9°%		7,818	226,454	2004
•	13	12	11	10	9	8	7	6	5	4	3	2	1		1) Dev.Yr. k
	-115	1,254	320	-761	5,840	4,873	41,581	61,208	156,143	272,364	283,169	228,341	86,904		2) S+k
	41,020	98,567	159,507	222,541	283,797	341,028	432,165	529,090	696,111	844,605	1,010,015	1,238,254	1,464,708	from (B)	3) v <sub>+k</sub>
	-0.3%	1.3%	0.2° %	-0.3%	2.1%	1.4° o	9.6°%	11.6%	22.4%	32.2° n	28.0° o	18.4°'i	5.9%	(2)/(3)	4) m <sub>k</sub>
	23,421.1	52,628.0	82,092.7	110,810.3	153,186.4	212,172.2	330,553.2	524,992.9	765,653.0	905,976.9	1,028,926.9	1,143,046.4	1,256,273.4	from (G)	5) (vr*)**
Tai	-0.5%	2.4%	0.4°%	-0.7%	3.8%	2.3%	12.6%	11.7%	20.4° %	30.1%	27.5°%	20.0°.6	6.9°%	(2)/(5)	6) m <sub>k</sub>
	0.1%	0. <b>2</b> %	0.5%	1.0%	2.0° %	5.0%	12.6° 6	11.7%	20.4%	30.1%	27.5%	20.0°%	6.9%	selected	7) m <sub>k</sub> *
1	137.9%	137.8°%	137.6%	137.1%	136.1%	134.1%	129.1%	116.5°%	104.9%	84.5° k	54.4"%	26.9° %	6.9°%		8) Σ(7)
1	100.0%	99.9°%	99.8%	99.4° a	98.7%	97.2%	93.6°%	84.5%	76.0%	61.3°%	39.5%	19.5%	5.0°%	(8)/(8#)	ο) b <sub>k</sub>

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### **Reserve Calculation for Incurred Data**

fr	
1	
1 1 1 1	
1	

(B)	(C)		(D)	(E)	(F)	(G)		· (II)	(1)	0)	(K)	(1.)	(M)
v,	С.,,,+1-1		∑mk	fi	ri‡	v,r,*		4	Ui	1-b <sub>n+1-i</sub>	R,	post. U <sub>r</sub>	post. ULR
			from (4)	(C)/(B)/(D)	selected	(B)*(E)		(ŀ)*(8#)	<u>(B)*([J)</u>	from (9)	ወ*ወ	_(C)+(K)	<u>(L)/(B)</u>
41.020	28,781		114.5°%	0.61	0.57	23.421.1		78.7° o	32,299.9	3.5°%	1,118.6	29,899.6	72.9%
57,547	35,826		114.5° •	0.54	0.51	29,206.9		70.0°.	40,279.1	4.9° .	1,979.1	37,805.1	65.7°%
60,940	35,181		113.1°%	0.51	0.48	29,464.7		66.7%	40,634.6	6.4%	2,585.8	37,766.8	62.0°%
63,034	33,508		112.1"%	0.47	0.46	28,717.6		62.8%	39,604.3	8.5° 'n	3,381.8	36,889.8	58.5"
61,256	49,909		111.3%	0.73	0.69	42,376.1		95.4° •	58,440.6	12.2%	7,109.0	57,018.0	93.1°%
57,231	67,286		108.3°%	1.09	1.03	58,985.8		142.1°6	81,346.9	17.2° %	14,024.5	81,310.5	142.1° •
91,137	116,520		102.7%	1.24	1.30	118,381.1		179.1°6	163,258.7	25.2°%	41,168.2	157,688.2	173.0° n
96,925	173,997		89.6%	2.00	2.01	194,439.7		276.7°'s	268,150.6	37.6"	100,850.1	274,847.1	283.6°%
167,021	177,864		75.1°%	1.42	1.44	240,660.2		198.7°%	331,893.1	48.2°%	160,000.6	337,864.6	202.3%
148,494	67,851		52.4°%	0.87	0.94	140,323.8		130.3%	193,519.8	63.2°'s	122,259.5	190,110.5	128.0° •
165,410	29,643		24.3° •	0.74	0.74	122,950.0		102.5° a	169,559.7	82.2° i	139,350.9	168,993.9	102.2"
228,239	4,043		6.4°'o	0.28	0.50	114,119.5		69.0°%	157,381.6	94.9° o	149,426.8	153,469.8	67.2°%
226,454	2,411		0.7° «	1.44	0.50	113,227.0		69.0°°	156,150.7	99.4° u	155,171.6	157,582.6	69.6° 5
	1	2	3	4	5	6		8		10	11	12	13
	10.864			-	158.05)		56 495						-1
from (B)				,					,	,			41,020
• • •				, .				,		,	· ·	,	
(2)/(3)	0.7%	5.6" •	17.9%	28.1%	22.7%	14.5" •	13.1%	5.6%	2.9%	0.8%	1.1%	1.4‴o	0.0° 6
from (G)	1,256,273.4	1,143,046.4	1,028,926.9	905,976.9	765,653.0	524,992.9	330,553.2	212,172.2	153,186.4	110,810.3	82,092.7	52,628.0	23,421.1
(2)/(5)	0.9°%	6.1%	17.6%	26.2° .	20.6%	14.6° 'n	17.1° o	9.0° 'n	5.5%	1.6%	2.0°%	2.6°%	0.0%
selected	0.9° is	6.1**	17.6° •	26.2°%	20.6° •	14.6%	17.1%	11.0%	7.0°%	5.0%	3.0%	2.0° 'n	2.0%
	0.9° •	7.0° •			71.4%	86.0° •		114.1%	121.1**	126.1°	129.1%	131.1%	133.1%
(8)/(8#)													96.5°%
	41,020 57,547 60,940 63,034 61,256 57,231 91,137 96,925 167,021 148,494 165,410 228,239 226,454 from (B) (2)/(3) from (G) (2)/(5)	41,020 28,781 57,547 35,826 60,940 35,181 61,256 49,909 57,231 67,286 91,137 116,520 96,925 173,997 167,021 177,864 148,494 67,851 165,410 29,643 228,239 4,043 228,239 4,043 226,454 2,411 108,864 from (B) 1,464,708 (2)/(3) 0.7°5 from (G) 1,256,273.4 (2)/(5) 0.9°5	41,020 28,781 57,547 35,826 60,940 35,181 63,034 33,508 61,256 49,909 57,231 67,286 91,137 116,520 96,925 173,997 167,021 177,864 148,494 67,851 165,410 29,643 228,239 4,043 228,454 2,411 1 2 10,864 69,792 from (B) 1,464,708 1,238,254 (2)/(3) 0.7% 5.6% from from (G) 1,256,273.4 1,143,046.4 (2)/(5) 0.9% 6.1% 0.9% 6.1%	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$

Exhibit C

Parameter Estimation for Bornhuetter/Ferguson

Tail-ILR 4.8° a

137.9%

100.0°°

### **Reserve Calculation for Paid Data**





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Exhibit E

Parameter Estimation for Bornhuetter/Ferguson